

SOLUTION

EXAM 2

CM3120

SPRING 2019 MORRISON

1. (20 points) Dimensional analysis is an important technique we introduce when we wish to understand very complex systems. For three of the following dimensionless numbers that arise in momentum or heat transfer give the following two pieces of information a) the formula for the definition of the quantity and b) a sentence indicating the significance of this dimensionless quantity.
- a. Reynolds number
 - b. Nusselt number
 - c. Biot number
 - d. Peclet number
 - e. Prandtl number

SOLUTION:

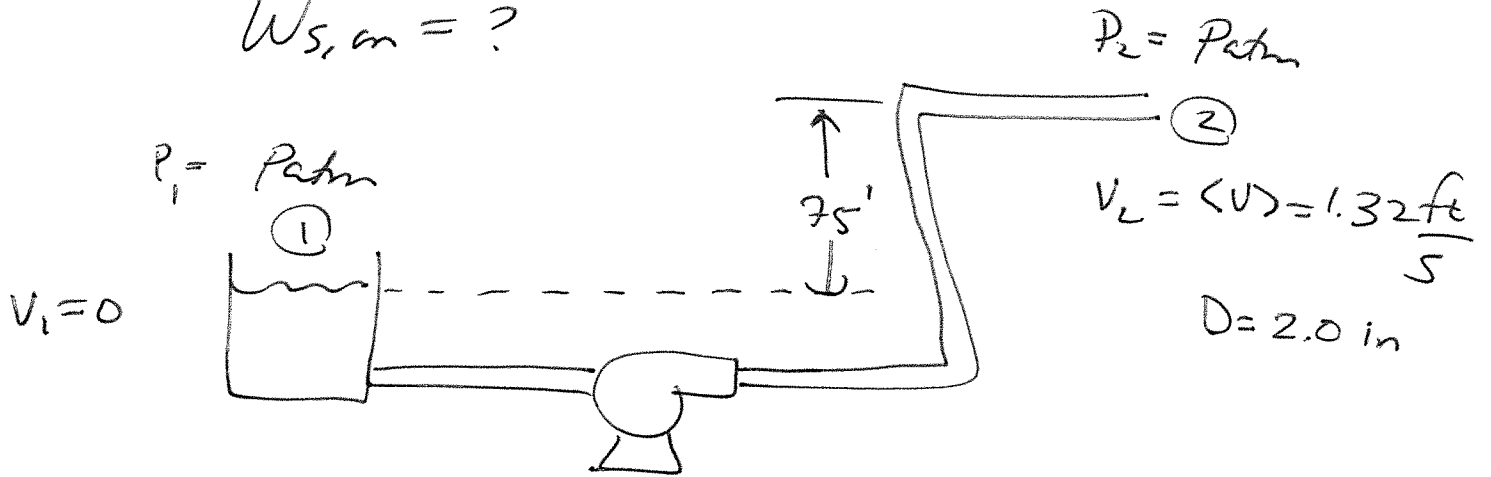
- a. **Reynolds number:** $Re = \frac{\rho V D}{\mu}$
Reynolds number appears in the non-dimensionalization of the microscopic momentum balance; it represents the ratio of inertial and viscous forces in a flow
- b. **Nusselt number:** $Nu = \frac{hD}{k}$
Nusselt number is the dimensionless heat transfer coefficient in forced convection flows.
- c. **Biot number:** $Bi = \frac{hD}{k}$
Reynolds number appears in the non-dimensionalization of unsteady state heat transfer solutions; it represents the ratio of external resistance to heat transfer (h) to internal resistances to heat transfer (k).
- d. **Peclet number:** $Pe = \frac{\hat{C}_p \rho V D}{k} = \frac{VD}{\alpha} = PrRe$
Peclet number appears in the non-dimensionalization of the microscopic energy balance; it represents the ratio of convective heat-transfer effects and conductive heat-transfer effects in a problem.
- e. **Prandtl number:** $Pr = \frac{\hat{C}_p \mu}{k} = \frac{\nu}{\alpha}$
Prandtl number appears as part of the Peclet number and along with Reynolds number appears in data correlations for dimensionless heat transfer coefficient, Nusselt number. The Peclet number represents the ratio of a materials ability to hold and store energy (\hat{C}_p) and the rate of its ability to conduct energy (k).

(2)

2. water
25°C

$$\frac{F}{g} = 4.2 \text{ ft}$$

$$W_{s,m} = ?$$



MECHANICAL ENERGY BALANCE

$$\frac{P_2 - P_1}{\rho} + \frac{V_2^2 - V_1^2}{2\alpha} + g(z_2 - z_1) + F = \frac{W_{s,m}}{m}$$

\swarrow both atmospheric \swarrow $\alpha = 1$ turbulent

$$\left(\frac{1.32 \text{ ft}}{\text{s}}\right)^2 \left(\frac{1}{2}\right) + \left(\frac{32.174 \text{ ft}}{\text{s}^2}\right)(75 \text{ ft}) + (4.2 \text{ ft})\left(\frac{32.174 \text{ ft}}{\text{s}^2}\right) = \frac{W_{s,m}}{m}$$

(3)

$$0.8712 + 2413.05 + 135.1308 = \frac{W_{s,m}}{\dot{m}}$$

$$\frac{W_{s,m}}{\dot{m}} = 2549.052 \frac{ft^2}{s^2}$$

↖
?

$$\dot{m} = Q_p = \langle v \rangle (\pi R^2) \rho$$

$$R = \frac{1}{12} ft$$

$$\rho = 62.25 \frac{lb_m}{ft^3}$$

$$\dot{m} = \left(1.32 \frac{ft}{s} \right) \left(\pi \left(\frac{1}{12} \right)^2 ft^2 \right) \left(62.25 \frac{lb_m}{ft^3} \right)$$

$$\dot{m} = 1.79267 \frac{lb_m}{s}$$

④

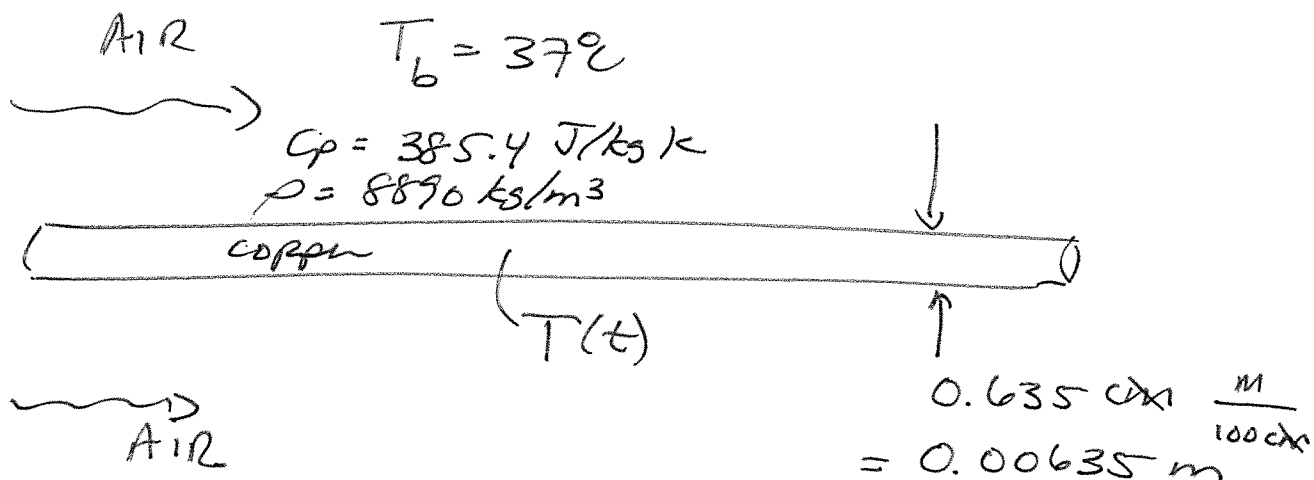
$$W_{s,m} = \left(2549.052 \frac{ft^2}{s^2} \right) \left(\frac{1.79267 \cancel{lbm}}{s} \right) \frac{\cancel{ft} / lb_f}{32.174 \frac{ft}{lb_f \cdot s^2}}$$

$$= 142.028 \text{ ft } lb_f / s$$

$$= \boxed{140 \frac{ft \cdot lb_f}{s}}$$

(5)

3.



$$t < 0, T = 7^\circ\text{C}$$

$$t \geq 0 \text{ in air w/ } h = 150 \frac{\text{W}}{\text{m}^2\text{K}}$$

$$V = \pi R^2 L = \frac{\pi D^2}{4} L$$

$$A = \pi D L$$

How long for $T \rightarrow 36^\circ\text{C}$?

MACRO UNSTEADY E-BAL

- no potential, kinetic energy effects

- no flow $\Rightarrow \Delta H = 0$

- no shafts $\Rightarrow W_{s,m} = 0$

$$\frac{dU}{dt} = \dot{Q}_{in} = h A (T_b - T) = \rho V \hat{c}_p \frac{dT}{dt}$$

We know the soln:

6

$$\ln \left(\frac{T_{\infty} - T}{T_D - T_0} \right) = - \frac{hA}{(\rho \hat{C}_p V)} t$$

$$\frac{hA}{\rho \hat{C}_p V} = \frac{h \pi D L}{\rho \hat{C}_p \frac{\pi D^2}{4} L} = \frac{4h}{\rho \hat{C}_p D}$$

$$= \frac{(4) \left(150 \frac{\text{W}}{\text{m}^2 \text{K}} \right) \frac{\cancel{\text{m}}}{\cancel{\text{m}}}}{\left(8890 \frac{\text{kg}}{\text{m}^3} \right) \left(385.4 \frac{\text{J}}{\text{kg K}} \right) (0.00635 \text{m})}$$

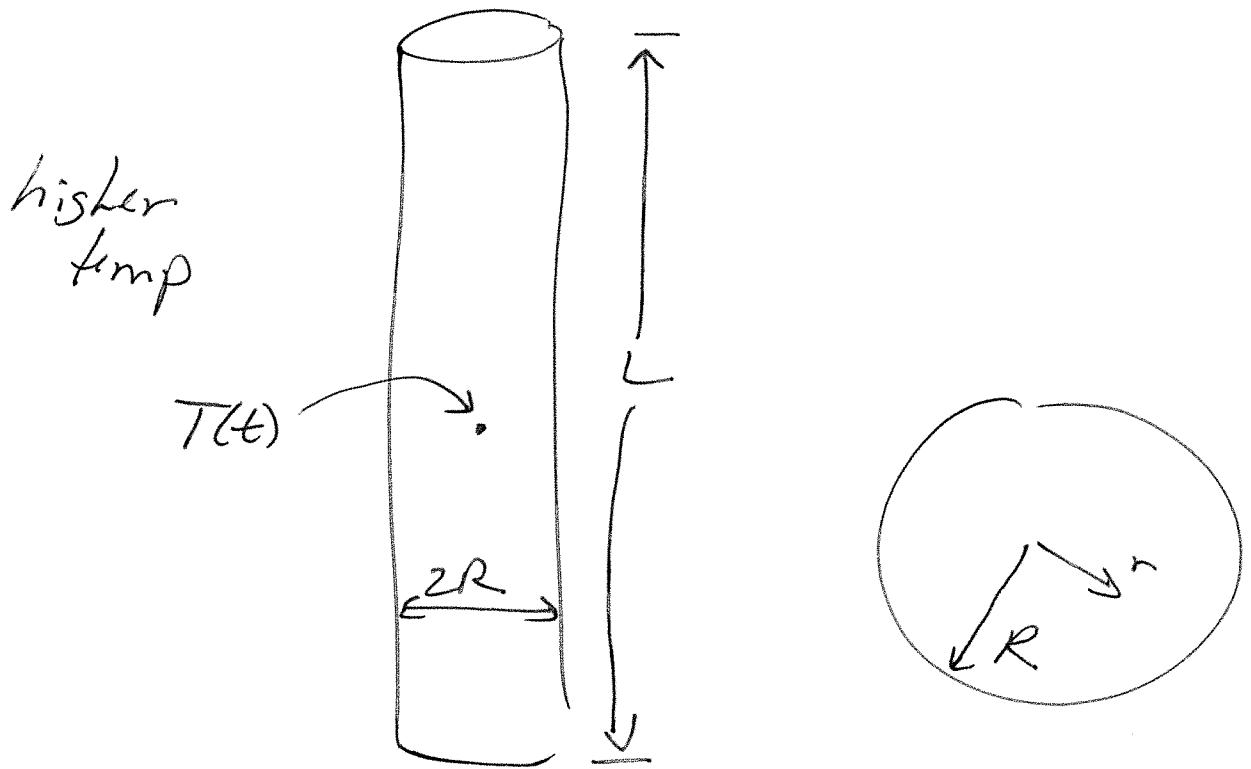
$$= 0.0275781 \text{ s}^{-1}$$

$$\ln \left(\frac{37 - 36}{37 - 7} \right) = - \frac{0.0275781}{\text{s}} t$$

$$t = 123.3 \text{ s} = \boxed{120 \text{ s}} = \boxed{2 \text{ min}}$$

4)

7



$$t \leq 0 \quad T = T_{\text{bath}}$$

$$t \geq 0 \quad T = T(t) \text{ in fluid w h } T_{\text{bulk}} = T_{\text{new}}$$

MICROSCOPIC ENERGY BALANCE:

(see sheet)

The Equation of Energy for systems with constant k

Microscopic energy balance, constant thermal conductivity; Gibbs notation

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + \underline{v} \cdot \nabla T \right) = k \nabla^2 T + S$$

Microscopic energy balance, constant thermal conductivity; Cartesian coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_x \frac{\partial T}{\partial x} + v_y \frac{\partial T}{\partial y} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{\partial^2 T}{\partial x^2} + \frac{\partial^2 T}{\partial y^2} + \frac{\partial^2 T}{\partial z^2} \right) + S$$

Microscopic energy balance, constant thermal conductivity; cylindrical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + v_z \frac{\partial T}{\partial z} \right) = k \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) + \frac{1}{r^2} \frac{\partial^2 T}{\partial \theta^2} + \frac{\partial^2 T}{\partial z^2} \right) + S$$

Microscopic energy balance, constant thermal conductivity; spherical coordinates

$$\rho \hat{C}_p \left(\frac{\partial T}{\partial t} + v_r \frac{\partial T}{\partial r} + \frac{v_\theta}{r} \frac{\partial T}{\partial \theta} + \frac{v_\phi}{\sin \theta} \frac{\partial T}{\partial \phi} \right) = k \left(\frac{1}{r^2} \frac{\partial}{\partial r} \left(r^2 \frac{\partial T}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left(\sin \theta \frac{\partial T}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 T}{\partial \phi^2} \right) + S$$

long
(no end
effects)

no
elec.
current;

no
radial

Symmetry
with respect
to θ

$$\Rightarrow \rho \hat{C}_p \frac{\partial T}{\partial t} = k \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) \right)$$

Reference: F. A. Morrison, "Web Appendix to *An Introduction to Fluid Mechanics*," Cambridge University Press, New York, 2013. On the web at www.chem.mtu.edu/~fmorriso/IFM_WebAppendixCD2013.pdf

E-BA2

9

$$\rho \hat{C}_p \frac{\partial T}{\partial t} = k \left(\frac{1}{r} \frac{\partial}{\partial r} \left(r \frac{\partial T}{\partial r} \right) \right)$$

initial condition:

IC: $t = 0 \quad T = T_{\text{both}} \quad \text{for all } r$

boundary conditions:

BC1

$$r = 0 \quad \frac{dT}{dr} = 0 \quad \text{for all } t > 0$$

$r = R$ Newton's law of cooling:

$$-k \frac{dT}{dr} = \frac{q_r}{A} = h (T - T_{\text{new}})$$

$\underbrace{\quad}_{>0} \quad \underbrace{\quad}_{<0} \quad \underbrace{\quad}_{<0}$

Since $T_{\text{new}} > T_{\text{both}}$

$\frac{q_r}{A} < 0$ (heat goes in negative "r" direction)

(10)

2nd BC:

$$r=R \quad -k \frac{dT}{dr} = h(T - T_{\text{new}})$$

for all $t > 0$

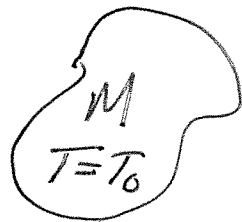
//

brass

$t < 0$

(11)

S)



HOT

$S = \text{surface area}$



COOLING
IN AIR

~ AIR ~
 $T = T_{\text{bulk}}$

MACRO UNSTEADY ENERGY BALANCE
System = the part itself

Assume: - no flow (it's solid) $\Rightarrow \Delta H = 0$
 $\Delta E_k = \Delta E_p = 0$

- kinetic + potential energy of the part are negligible
- no shafts \Rightarrow no shaft work

$$\frac{dU_{sys}}{dt} = \dot{Q}_{in} = \sum_i \dot{Q}_{in,i}$$

$$\dot{M} C_v \frac{dT}{dt}$$

↑
rad.

- no conduction
- no current
- no reaction
- yes convection
- yes radiation

$$\dot{M} C_p \frac{dT}{dt} = h S (T_{bulk} - T)$$

?
make
as big as
reasonable
⇒ 250 W/m²K

$$+ \sum \sigma S (T_{bulk}^4 - T^4)$$

? = 0.22 (see
Table)
Engineering
Toolbox)

brass:

$$C_p = 381.2 \frac{J}{kg \cdot K}$$

$$h = 250 \text{ W/m}^2 \text{ K}$$

$$\sigma = 5.674 \times 10^{-8} \frac{W}{m^2 K^4}$$

this is the
high end
for forced
convection
in gases
(see Table)