

✓ Module 3 (done)

CM3120: Module 3

Diffusion and Mass Transfer I

- ✓ Introduction to diffusion/mass transfer
- ✓ Classic diffusion and mass transfer—Quick Start a): 1D Evaporation
- ✓ Classic diffusion and mass transfer—Quick Start b): 1D Radial droplet
- ✓ Cycle back: Fick's mass transport law
- ✓ Microscopic species A mass balance
- ✓ Classic diffusion and mass transfer—c): 1D Mass transfer with chemical reaction

Module 4: Take Stock

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Unit Operations

The term “unit operation” was coined by the founders of chemical engineering in the late 1800s.

Chemical processes may be broken down into basic steps that bring about physical or chemical change. These steps are called “unit operations.”

Chemical engineering unit operations may be divided into six classes:

1. **Fluid flow processes** including fluids transportation, filtration, mixing, and solids fluidization.
2. **Heat transfer processes** including evaporation, heat exchange, ovens/furnaces.
3. **Mass transfer processes** including gas absorption, distillation, extraction, adsorption, membrane separation, crystallization & drying
4. **Thermodynamic processes** including refrigeration, water cooling, and gas liquefaction.
5. **Reaction** including homogeneous and catalytic reactors
6. **Mechanical processes** including solids transportation, crushing & pulverization, and screening & sieving.

Ref: <https://www.sciencehistory.org/historical-profile/arthur-d-little-william-h-walker-and-warren-k-lewis>

Ref: Wikipedia, Unit Operations

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Unit Operations

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Ref: Wikipedia, Unit Operations © Faith A. Morrison, Michigan³ Tech U.

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Unit Operations

Are each characterized by a dominant physics “unit operation” was coined by the founders of chemical engineering in the late 1800s.

Chemical processes may be broken down into **These “basic steps”** about physical or chemical change. These steps are called “unit operations.”

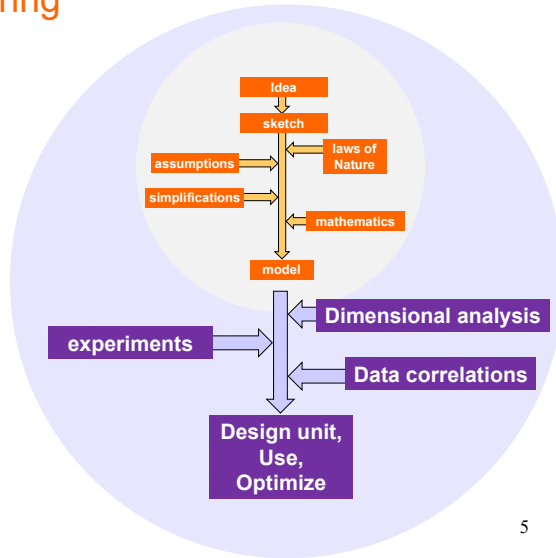
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Pulling together the physics (how the world works) for these units is the subject of the field of chemical engineering

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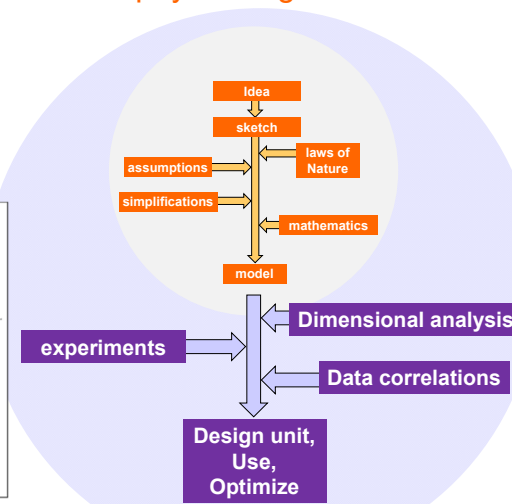


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Let's get specific

How does this process work for units dominated by mass transfer?

Process for pulling the physics together for a unit



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Species A Mass Transfer Processes

Engineering Purposes:

- Distillation
- Gas absorption
- Extraction
- Membrane separation



Knowledge and Skills

1. Continuum, mixtures
2. Mass, species A mass, energy balances, fluid flow fundamentals
3. Species A flux \propto concentration gradient
4. Transfers at boundaries, k_x
5. Dimensional analysis and data correlations Nu_{AB} , Sh
6. Thermo: Binary phase equilibria
7. Classics: Stagnant layers, constant molar overflow, equimolar counter diffusion, film model, penetration model, boundary layers

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Species A Mass Transfer Processes

Engineering Purposes:

- Distillation
- Gas absorption
- Extraction
- Membrane separation

Modules 3, 4 will cover these topics for species A mass transfer

Knowledge and Skills

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Species A Mass Transfer Processes

Module 3

Module 4

Friday Project

Knowledge and Skills

1. Continuum, mixtures
2. Mass, species A mass, energy balances, fluid flow fundamentals
3. Species A flux \propto concentration gradient
4. Transfers at boundaries, k_x
5. Dimensional analysis and data correlations Nu_{AB} , Sh
6. Thermo: Binary phase equilibria
7. Classics: Stagnant layers, constant molar overflow, equimolar counter diffusion, film model, penetration model, boundary layers

Engineering Purposes:

- Distillation—CMO
- Gas absorption—penetration model
- Extraction
- Membrane separation

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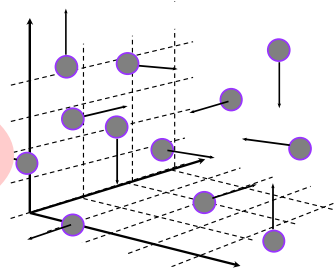
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CM3120: Module 4

Diffusion and Mass Transfer II

- I. Classic diffusion and mass transfer: d) EMCD
- II. Classic diffusion and mass transfer: e) Penetration model
- III. Unsteady macroscopic species A mass balances (Intro)
- IV. Interphase species A mass transfers—To an interface— k_x, k_c, k_p
- V. Unsteady macroscopic species A mass balances (Redux)
- VI. Interphase species A mass transfers—Across multiple resistances— K_L, K_G
- VII. Dimensional analysis
- VIII. Data correlations

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CM3120: Module 4**Module 4 Lecture I
Classics Diffusion &
Mass Transfer
(EMCD)**

Professor Faith A. Morrison

Department of Chemical Engineering
Michigan Technological University

www.chem.mtu.edu/~fmorriso/cm3120/cm3120.html

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1D Steady Diffusion

**Classic 1D Steady Diffusion
Summary**

- a. 1D rectangular mass transfer (evaporating tank, **Ex 1**)
- b. 1D radial mass transfer (evaporating droplet, **Ex 2**)
- c. Heterogeneous chemical reaction (catalytic converter, **Ex 3**)
- d.

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Introduction to Diffusion and Mass Transfer in Mixtures QUICK START

Recurring Modeling Assumptions in Diffusion (“Classics”)

- Near a liquid-gas interface, the region in the gas near the liquid is a film where slow diffusion takes place
- The vapor near the liquid-gas interface is often saturated (Raoult’s law, $x_A = p_A^*/p$)
- If component A has no sink, flux $\underline{N}_A = 0$.
- If A diffuses through stagnant B , $\underline{N}_B = 0$.
- If A is dilute in B , we can neglect the convection term ($N_{Az} = J_{Az}^*$)
- Because diffusion is slow, we can make a quasi-steady-state assumption
- If, for example, two moles of A diffuse to a surface at which a rapid, irreversible reaction converts it to one mole of B , then at steady state $-0.5\underline{N}_A = \underline{N}_B$.
- Homogeneous reactions appear in the mass balance; heterogeneous reactions appear in the boundary conditions and relate fluxes
- If a binary mixture of A and B are undergoing steady equimolar counter diffusion, $\underline{N}_A = -\underline{N}_B$. (coming)

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1D Steady Diffusion

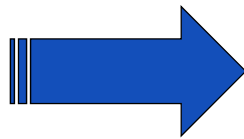
Classic 1D Steady Diffusion Summary

- a. 1D rectangular mass transfer (evaporating tank, **Ex 1**)
- b. 1D radial mass transfer (evaporating droplet, **Ex 2**)
- c. Heterogeneous chemical reaction (catalytic converter, **Ex 3**)
- Next:** d. Equimolar counter diffusion (distillation, $\underline{v}^* = 0$, $(\underline{N}_A = \underline{J}_A^*)$ **Ex 4**)

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We begin **Module 4** with discussion of **Distillation** and **Gas Absorption**, two unit operations in which mass transfer is a dominant physics.

Studying these units we encounter some additional classic models of mass transfer that have been found to be successful in describing the real behavior of these units (within limits).



Distillation

Mass Transfer in Distillation

Air separation distillation column

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Distillation

Mass transfer in Staged Distillation

Air separation distillation column

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Distillation

Distillation

Distillation is the process of separating the components of a liquid mixture by exploiting differences in the relative volatility of the mixture's components.

The classic separation produces a **distillate stream** (at the top) that is rich in the component with lower boiling point (higher volatility) and a **bottoms stream** that is rich in the component with higher boiling point (lower volatility).

In a distillation, column, because the components are *vaporized*, distillation is energy-intensive (expensive).

Distillation is the most common unit operation.

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McCabe-Thiele Method (review) REVIEW

A simplified model of **staged distillation** produces the McCabe-Thiele method of designing (sizing) distillation columns

Introduction to McCabe-Thiele Design Method: Binary Distillation

Professor Faith A. Morrison
 Department of Chemical Engineering
 Michigan Technological University
 30 January 2021

YouTube: DrMorrisonMTU
<https://youtu.be/ybPVpP15iiY>

(See YouTube video on my channel, Dr.MorrisonMTU)
 (separations course)

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McCabe-Thiele Method (review)

REVIEW

The McCabe-Thiele method assumes:
Equilibrium Stages

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McCabe-Thiele Method (review)

REVIEW

L_3, V_3 are assumed to be in equilibrium

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McCabe-Thiele Method (review)

REVIEW

L_3, V_3 are assumed to be in equilibrium

L_3, V_4 are passing streams linked by the operating line (mass balance on upper half of column)

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McCabe-Thiele Method (review)

REVIEW

The McCabe-Thiele method assumes:

Constant Molar Overflow (CMO)

Enriching section
 Liquid molar flow rates = L
 Vapor molar flow rates = V

Stripping section
 Liquid molar flow rates = \bar{L}
 Vapor molar flow rates = \bar{V}

Four conditions:

1. $\Delta \hat{H}_{vap}$ independent of mixture concentration
2. Latent heat dominates
3. Adiabatic column, $\dot{Q} = 0$
4. Saturated liquid and vapor lines on $\hat{H} - x_A$ diagram are parallel

We assumed upper section had common flows L, V

And lower section had common flows \bar{L}, \bar{V}

Enriching section
 Rectifying section
 Upper section

Stripping section
 Lower section

D
 x_D

B
 x_B

F
 x_F

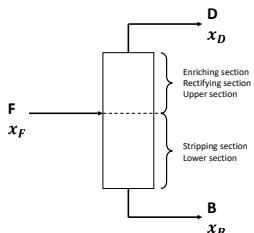
These assumptions have mass transfer implications

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McCabe-Thiele Method (review) REVIEW

McCabe-Thiele method

Goal: Determine the number of stages of a distillation column that can achieve the desired separation



Constraints

1. Overall mass conservation (mole balances)
2. Equilibrium stages
3. All stages above the feed satisfy the same mole balances drawn through D
4. All stages below the feed satisfy the same mole balances drawn through B
5. Upper and lower operating lines intersect at the feed tray
6. The quality q of the feed and mole balances on each phase at the feed tray close the calculation

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McCabe-Thiele Method (review) REVIEW

Summary of Constraints—McCabe-Thiele method

1. Overall mass conservation (mole balances)

$$F = D + B$$

$$x_F F = x_D D + x_B B$$
2. Equilibrium stages: data $y^* = f(x^*)$
3. Above the feed mole balances through D constrain **passing streams** $y(x)$ (upper operating line):

$$y = \left(\frac{L}{V}\right)x + \left(1 - \frac{L}{V}\right)x_D$$

We assume upper section has common flows L, V
4. Below the feed mole balances through B constrain **passing streams** $\bar{y}(\bar{x})$ (lower operating line)

$$\bar{y} = \left(\frac{\bar{L}}{\bar{V}}\right)\bar{x} - \left(\frac{\bar{L}}{\bar{V}} - 1\right)x_B$$

And lower section has common flows \bar{L}, \bar{V}
5. Upper and lower intersect at **feed tray**, $\tilde{y}(\tilde{x})$

$$\tilde{y} = \left(\frac{L - \bar{L}}{V - \bar{V}}\right)\tilde{x} + \frac{x_F F}{V - \bar{V}}$$
6. The quality q of the feed and mole balances on each phase at the feed tray close the calculation (q -line)

$$\tilde{y} = \left(\frac{q}{q - 1}\right)\tilde{x} + \frac{x_F}{1 - q}$$

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McCabe-Thiele Method (review) **REVIEW**

The total condenser starts the column calculation with an equilibrium stage; the information then passes to the passing streams (upper operating line), and then to the next equilibrium stage, etc. alternating until the feed is passed. At this point the passing streams are designated by the lower operating line, and the process continues until the bottoms composition is reached.

YouTube: DrMorrisonMTU
<https://youtu.be/ybPVpP15iiY>

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Mass Transfer in Distillation

Mass transfer in Distillation

In general, the molar flow rates throughout the enriching (L, V) and stripping (\bar{L}, \bar{V}) sections are not constant.

We can assume they are constant if every time a mole of vapor is condensed, a mole of liquid is vaporized (*Constant Molal Overflow*)

Constant Molal Overflow (CMO), used in McCabe-Thiele method

1. The heat of vaporization per mole $\Delta \hat{H}_{vap} = \lambda$ is constant (independent of concentration)
2. Specific heat changes are small compared to latent heat changes
3. The column is adiabatic, $\dot{Q} = 0$
4. (equivalent to 1+2) The saturated liquid and vapor lines on an enthalpy-composition diagram (in molar units) are parallel

Example 4: Mass transfer in Distillation

Distillation

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Mass Transfer in Distillation

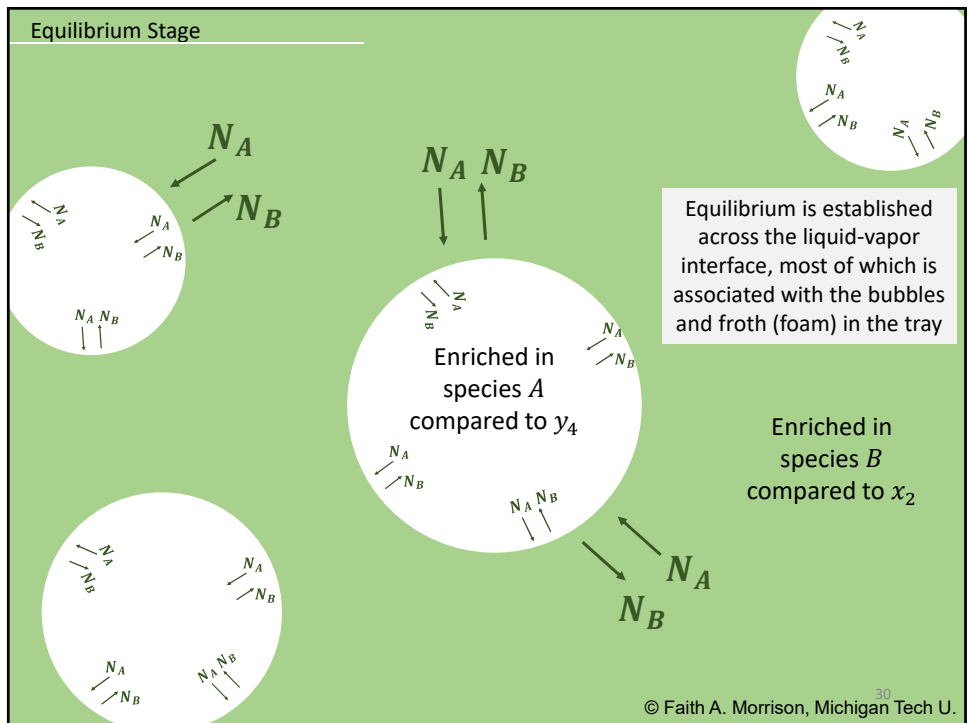
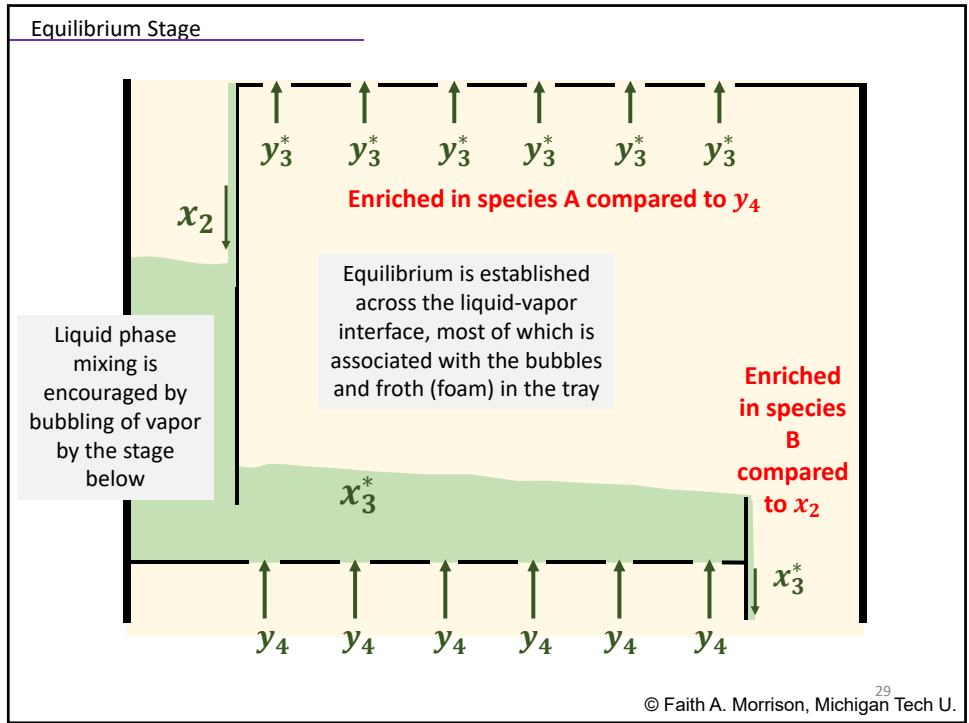
What is the mass transfer mechanism for constant molal overflow (CMO) and for the separation on the stage?

To answer, let's zoom in on an equilibrium stage

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Equilibrium Stage

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Mass Transfer in Distillation

A Picture of Mass Transfer in Distillation

The molar flow rates throughout the enriching (L, V) and stripping (\bar{L}, \bar{V}) sections are constant if:

This condition is met by **equimolar counter diffusion (EMCD)**.

Every time a mole of vapor is condensed, a mole of liquid is vaporized (**Constant Molal Overflow**)

$$v_A = -v_B$$

$$N_A = -N_B$$

Note:

$$N_A + N_B = cv^*$$

$$\Rightarrow v^* = 0$$

(Mod 3, lecture I)
Diffusion progresses at a rate of

- $\sim 5 \text{ cm/min}$ (gases)
- $\sim 0.05 \text{ cm/min}$ (liquids)
- $\sim 10^{-5} \text{ cm/min}$ (solids)

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Mass transfer in Distillation

Example 4: Mass transfer in distillation

Equimolar Counter Diffusion

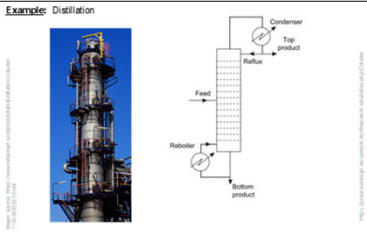
Example: Distillation

A distillation column is separating two components A and B at steady state. In the vapor phase of each equilibrium stage the two components are moving in **equimolar counter diffusion**. What are the molar fluxes of A and B in the vapor phase? What is the concentration distribution in the region of the equimolar counter diffusion?

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Mass transfer in Distillation

Example 4: Mass transfer in distillation



A distillation column is separating two components A and B at steady state. In the vapor phase of each equilibrium stage the two components are moving in equimolar counter diffusion. What are the molar fluxes of A and B in the vapor phase? What is the concentration distribution in the region of the equimolar counter diffusion?

Solve

See hand notes for the start (Example 4) HW4 Prob 2 (&7)

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Mass Transfer in Distillation

Example 4: Mass transfer in distillation

A distillation column is separating two components A and B at steady state. In the vapor phase of each equilibrium stage the two components are moving in equimolar counter diffusion. What are the molar fluxes of A and B in the vapor phase? What is the concentration distribution in the region of the equimolar counter diffusion?

Answers:

$$N_{Az} = \frac{P_{A1} - P_{A2}}{(z_2 - z_1)} \left(\frac{D_{AB}}{RT} \right) \quad \text{(constant flux proportional to } D_{AB} \text{)}$$

$$\frac{x_A - x_{A1}}{x_{A1} - x_{A2}} = \frac{z - z_1}{z_1 - z_2} \quad \text{(linear concentration profile)}$$

$$x_A = \left(\frac{x_{A1} - x_{A2}}{z_1 - z_2} \right) z - \frac{z_1(x_{A1} - x_{A2})}{z_1 - z_2} + x_{A1}$$

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1D Steady Diffusion—Equimolar Counter Diffusion

Problem Summary: Equimolar Counter Diffusion (EMCD)

- One-dimensional (1D)
- Steady
- Use molar flux (due to equimolar counter diffusion specified)
- Use combined molar flux \underline{N}_A or \underline{J}_A^*
- Boundary conditions: concentrations known over a known distance

Flux choice
Choose:

- **Molar** because *equimolar* motion was specified
- **Combined molar** and **molar** are the same when $\underline{v}^* = 0$ ($\underline{N}_A = \underline{J}_A^*$)

$$\underline{J}_A^* = c x_A (\underline{v}_A - \underline{v}^*)$$

$$\underline{N}_A = c_A \underline{v}_A$$

These two molar fluxes are the same when $\underline{v}^* = 0$.

1D Steady Diffusion—Equimolar Counter Diffusion

Example: Distillation (continued)

"This is only true if every time a mole of vapor is condensed, a mole of liquid is vaporized (Constant Molar Overflow)"

This condition is met by equimolar counter diffusion.

$\begin{matrix} A \\ \uparrow \\ E_A \\ \downarrow \\ B \end{matrix}$

$\begin{matrix} \uparrow \\ E_B \\ \downarrow \\ B \end{matrix}$

$$E_A = -E_B$$

$$v^* = x_A E_A + x_B E_B = 0$$

$$\underline{N}_A = -\underline{N}_B$$

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1D Steady Diffusion—Equimolar Counter Diffusion

Analysis:

Assuming EMCD for staged distillation implies linear concentration profile. And constant flux proportional to the diffusion coefficient

$$N_{Az} = \frac{P_{A1} - P_{A2}}{(z_2 - z_1) RT} \mathcal{D}_{AB}$$

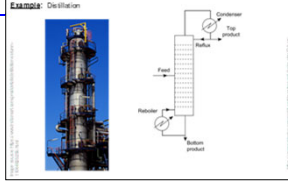
Since \mathcal{D}_{AB} is a **material property** of the AB pair, we can easily predict how a new distillation separation will perform (according to the proposed model, i.e. EMCD; but is it true?)

When we make a prediction, the next thing is to check and see if it is true. (Is the tray flux proportional to the diffusion coefficient? It's hard to measure the flux.)

Later we will define some macroscopic mass transfer methods that we can use to assess the degree to which EMCD seems consistent with measurements for distillation (mass transfer coefficients and how they depend on \mathcal{D}_{AB}).

For now, we can just hold onto EMCD as an idea of how mass transfer works in a distillation column.

Example: Distillation



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Mass Transfer in Distillation

How good are our modeling assumptions?

Mole fraction of A separated and sent up the column (equilibrium tray): $y_3^* - y_4$. This represents a likely overestimate of the amount of separation achieved.

If the tray is not at equilibrium, $y_3 < y_3^*$

Tray efficiency $\equiv \frac{y_3 - y_4}{y_3^* - y_4}$

Murphree efficiency

The *tray efficiency* is an issue of the **mass transfer limitations** in the separations process taking place.

(We'll return to this efficiency once we develop some more practical mass-transfer tools)

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1D Steady Diffusion

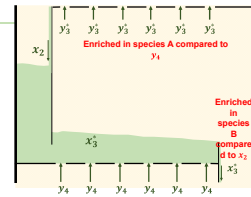
Classic 1D Steady Diffusion Summary

- 1D rectangular mass transfer (evaporating tank, **Ex 1**)
- 1D radial mass transfer (evaporating droplet, **Ex 2**)
- Heterogeneous chemical reaction (catalytic converter, **Ex 3**)
- Equimolar counter diffusion (distillation, $\underline{v}^* = 0$, $(\underline{N}_A = \underline{J}_A^*)$ **Ex 4**)
- More...

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Distillation modeling: EMCD

Distillation Modeling Summary



- Distillation modeling with **equilibrium stages** gives a plausible picture of the unit operation
- **Equimolar counter diffusion (EMCD)** is the mass transfer picture; this is consistent with constant molar overflow (CMO, McCabe Thiele analysis)
- EMCD is a “classic” of diffusion and mass transfer
- Distillation trays are **unlikely to be at equilibrium**; mass transfer limits the separation taking place on the trays; account for this with a **Murphree efficiency**
- Many (most?) columns these days are packed; we would have to consider a different model for packed columns

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