

Generalized Linear-Viscoelastic Model:
(strain version)

infinitesimal strain tensor

$$\underline{\underline{\tau}} = + \int_{-\infty}^t M(t-t') \underline{\underline{\gamma}}(t, t') dt'$$

$$M(t-t') \equiv \frac{\partial G(t-t')}{\partial t'}$$

memory function

It is the use of the infinitesimal strain tensor as the strain measure that causes the frame-variance in the GLVE model.

What's wrong w/

using $\underline{\delta}(t, t')$

as our strain measure?

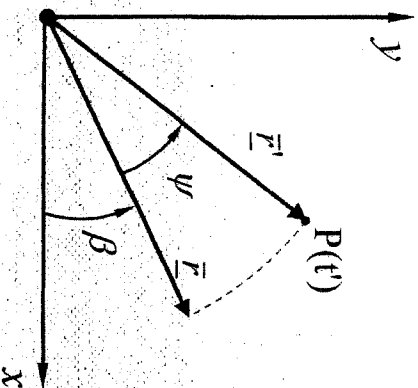
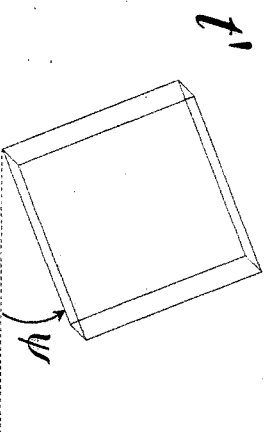
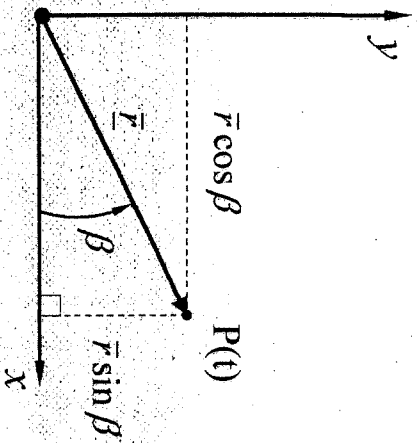
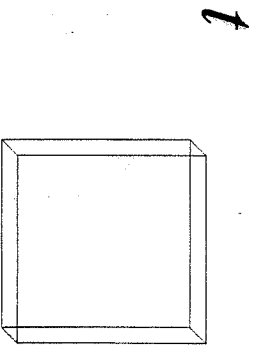
infinitesimal
strain tensor

Def $\underline{\delta}(t, t') = \nabla \underline{u}(t, t') + \left[\nabla \underline{u}(t, t') \right]^T$

$$\nabla \underline{u}(t, t') = \underline{r}(t') - \underline{r}(t)$$

difference
between
the position
vector for a
moving point
at two times

No stress is generated when a fluid is rotated;
what does the GLVE predict?



↓ reference time

$$\underline{r} = \underline{r}(t) = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{xyz} = \underline{\bar{r}} + z \hat{e}_z$$

$$\underline{r}' = \underline{r}(t') = \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}_{x'y'z'} = \underline{\bar{r}}' + z' \hat{e}_z$$

note: $z = z'$
 $|\underline{r}| = |\underline{r}'|$

Looking for $\underline{u} = \underline{r}' - \underline{r} = \underline{\bar{r}}' - \underline{\bar{r}}$

$$\underline{\bar{r}}' = \begin{pmatrix} \bar{r} \cos(\psi + \beta) \\ \bar{r} \sin(\psi + \beta) \\ 0 \end{pmatrix}_{x'y'z'}$$

$x = \bar{r} \cos \beta$
 $y = \bar{r} \sin \beta$

$$\underline{u}' = \begin{pmatrix} \bar{r} [\cos \psi \cos \beta - \sin \psi \sin \beta] \\ \bar{r} [\sin \psi \cos \beta + \cos \psi \sin \beta] \\ 0 \end{pmatrix}_{x'y'z'}$$

$$\underline{r}' = \begin{pmatrix} x \cos \psi - y \sin \psi \\ x \sin \psi + y \cos \psi \\ 0 \end{pmatrix}_{xyz}$$

$$\underline{r} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{xyz}$$

$$\underline{r} = \begin{pmatrix} x \\ y \\ 0 \end{pmatrix}_{xyz}$$

$$\underline{u} = \underline{r}' - \underline{r} = \underline{r}' - \underline{r}$$

$$\underline{u} = \begin{pmatrix} (\cos \psi - 1)x - y \sin \psi \\ x \sin \psi + y(\cos \psi - 1) \\ 0 \end{pmatrix}_{xyz}$$

$$\nabla \underline{u} + (\nabla \underline{u})^T = \underline{\underline{\gamma}}$$

Carrying out this calculation we obtain:

$$\underline{\underline{\gamma}} = \begin{pmatrix} 2(\cos \psi - 1) & 0 & 0 \\ 0 & 2(\cos \psi - 1) & 0 \\ 0 & 0 & 0 \end{pmatrix}_{xyz}$$

GLVE Prediction for Rigid-Body Rotation around the z-axis

$$\underline{\underline{\tau}} = + \int_{-\infty}^t M(t-t') \begin{pmatrix} 2(\cos\psi - 1) & 0 & 0 \\ 0 & 2(\cos\psi - 1) & 0 \\ 0 & 0 & 0 \end{pmatrix}_{xyz} dt'$$

Why does GLVE make this erroneous prediction?

$$\underline{\underline{\gamma}}(t, t') = \nabla \underline{u}(t, t') + [\nabla \underline{u}(t, t')]^T$$

$$\underline{u}(t, t') = \underline{r}(t') - \underline{r}(t)$$

Because this vector, while accounting for deformation, *also accounts for changes in orientation.*

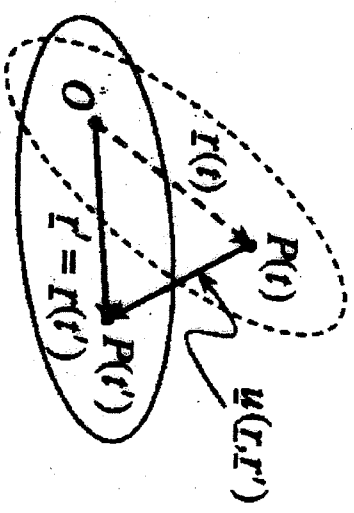
$$\underline{r}(t, t') = \nabla \underline{u}(t, t') + [\nabla \underline{u}(t, t')]^T \underline{r}(t, t')$$

$$\underline{u}(t, t') = \underline{r}(t') - \underline{r}(t)$$

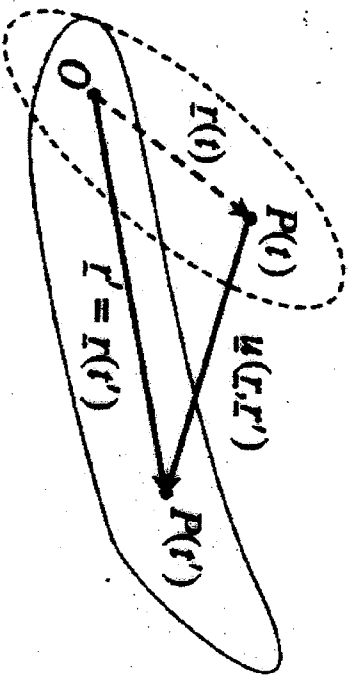
Accounts for changes in shape and orientation.

$$\underline{u}(t, t') = \underline{r}' - \underline{r}$$

Origin O fixed in space



Orientation changes
(\underline{r} changes direction)
Shape does not change
(length of \underline{r} does not change)



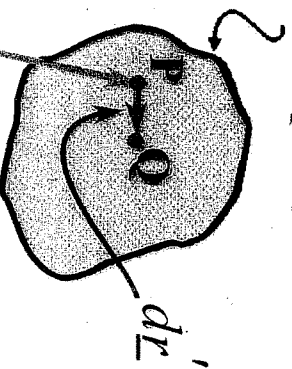
Orientation changes
Shape changes

We desire a strain tensor that accurately captures large-strain deformation without being affected by rigid-body rotation.

Consider:

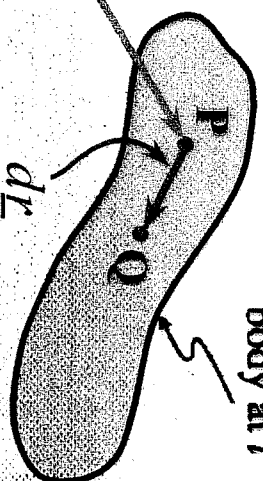
$time = t'$

Shape and position of a deforming body at t'



$time = t$

Shape and position of the same deforming body at t



fixed coordinate system (XYZ)

⇒ consider the position of a particle at time t'

To identify which particle I'm talking about, I'll use its position at t

$\underline{r}'(t', \underline{r}) =$ position at t' of the particle that at t was at position \underline{r}

$$\underline{r}' = \begin{pmatrix} x' \\ y' \\ z' \end{pmatrix}_{x'y'z'}$$

$$\underline{r} = \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{xyz}$$

$$d\underline{r}' = \begin{pmatrix} dx' \\ dy' \\ dz' \end{pmatrix}_{x'y'z'}$$

write using chain rule

$$\underline{r}' = \underline{r}'(t', \underline{r})$$

$$dx' = \frac{\partial x'}{\partial x} dx + \frac{\partial x'}{\partial y} dy + \frac{\partial x'}{\partial z} dz$$

$$dy' = \frac{\partial y'}{\partial x} dx + \frac{\partial y'}{\partial y} dy + \frac{\partial y'}{\partial z} dz$$

$$dz' = \frac{\partial z'}{\partial x} dx + \frac{\partial z'}{\partial y} dy + \frac{\partial z'}{\partial z} dz$$

NOTE - this can be written as,

$$dx' = \frac{\partial x'}{\partial r} \cdot d\underline{r}$$

$$= \frac{\partial x'}{\partial x_i} \underbrace{\hat{e}_i}_{\delta_{ip}} \cdot dx_p \hat{e}_p = \frac{\partial x'}{\partial x_p} dx_p$$

$$dy' = \frac{\partial y'}{\partial r} \cdot d\underline{r}$$

$$dz' = \frac{\partial z'}{\partial r} \cdot d\underline{r}$$

OR

$$\underline{dr}' = \frac{\partial \underline{r}'}{\partial \underline{r}} \cdot d\underline{r}$$

$$\underline{dr}' = \underline{F} \cdot d\underline{r}$$

Let \underline{F}^{-1} be the inverse of \underline{F}

$$\underline{dr}' = \underline{F} \cdot \underline{dr}$$

$$\underline{F}^{-1} \cdot \underline{F} = \underline{I}$$

$$\underline{F} \cdot \underline{F}^{-1} = \underline{I}$$

$$\underline{F}^{-1} \cdot \underline{dr}' = \underbrace{\underline{F}^{-1} \cdot \underline{F}}_{\underline{I}} \cdot \underline{dr}$$

$$\underline{F}^{-1} \cdot \underline{dr}' = \underline{dr}$$

↑
inverse
deformation
gradient tensor

compare:

$$\underline{F} \cdot \underline{dr} = \underline{dr}'$$

Deformation-
gradient tensor

$$\underline{\underline{F}}(t, t') \equiv \frac{\partial \underline{r}'}{\partial \underline{r}} = \frac{\partial r'_i}{\partial r_p} \hat{e}_p \hat{e}_i = \begin{pmatrix} \frac{\partial x'}{\partial x} & \frac{\partial y'}{\partial x} & \frac{\partial z'}{\partial x} \\ \frac{\partial x'}{\partial y} & \frac{\partial y'}{\partial y} & \frac{\partial z'}{\partial y} \\ \frac{\partial x'}{\partial z} & \frac{\partial y'}{\partial z} & \frac{\partial z'}{\partial z} \end{pmatrix}_{xyz}$$

Inverse deformation-
gradient tensor

$$\underline{\underline{F}}^{-1}(t', t) \equiv \frac{\partial \underline{r}}{\partial \underline{r}'} = \frac{\partial r_m}{\partial r'_j} \hat{e}_j \hat{e}_m = \begin{pmatrix} \frac{\partial x}{\partial x'} & \frac{\partial y}{\partial x'} & \frac{\partial z}{\partial x'} \\ \frac{\partial x}{\partial y'} & \frac{\partial y}{\partial y'} & \frac{\partial z}{\partial y'} \\ \frac{\partial x}{\partial z'} & \frac{\partial y}{\partial z'} & \frac{\partial z}{\partial z'} \end{pmatrix}_{xyz}$$

© Faith A. Morrison, Michigan T

25' 

EXAMPLE: What is the inverse-deformation gradient tensor in steady shear flow?

$$\underline{v} = \begin{pmatrix} \dot{\gamma}_0 y \\ 0 \\ 0 \end{pmatrix}_{xyz}$$

$$\underline{r} = \begin{pmatrix} x' + (t - t')\dot{\gamma}_0 y' \\ y' \\ z' \end{pmatrix}_{xyz}$$

© Faith A. Morrison, Michigan

35 7 ~~7~~

Calculate F , F^{-1} for shear
 time dif. velocity

$$1 \rightarrow \begin{pmatrix} x \\ y \\ z \end{pmatrix}_{xyz} = \begin{pmatrix} x' + (t-t')\dot{\gamma}_0 y' \\ y' \\ z' \end{pmatrix}_{x'y'z'}$$

$$F = \frac{\partial \underline{r}}{\partial \underline{r}'} = \begin{pmatrix} \frac{\partial x}{\partial x'} & \frac{\partial y}{\partial x'} & \frac{\partial z}{\partial x'} \\ \frac{\partial x}{\partial y'} & \frac{\partial y}{\partial y'} & \frac{\partial z}{\partial y'} \\ \frac{\partial x}{\partial z'} & \frac{\partial y}{\partial z'} & \frac{\partial z}{\partial z'} \end{pmatrix}_{xyz}$$

Need to invert this

$$\begin{aligned} x' + (t-t')\dot{\gamma}_0 y' &= x \\ y' &= y \\ z' &= z \end{aligned}$$

SOLVE FOR
 x', y', z'

tensor	shear in 1-direction with gradient in 2-direction	uniaxial elongation in 3-direction	ccw rotation around \hat{e}_3
$\underline{\underline{F}}(t, t')$	$\begin{pmatrix} 1 & 0 & 0 \\ -\gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{\frac{\epsilon}{2}} & 0 & 0 \\ 0 & e^{\frac{\epsilon}{2}} & 0 \\ 0 & 0 & e^{-\epsilon} \end{pmatrix}_{123}$	$\begin{pmatrix} \cos \psi & -\sin \psi & 0 \\ \sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$
$\underline{\underline{F}}^{-1}(t', t)$	$\begin{pmatrix} 1 & 0 & 0 \\ \gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{-\frac{\epsilon}{2}} & 0 & 0 \\ 0 & e^{-\frac{\epsilon}{2}} & 0 \\ 0 & 0 & e^{\epsilon} \end{pmatrix}_{123}$	$\begin{pmatrix} \cos \psi & \sin \psi & 0 \\ -\sin \psi & \cos \psi & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$
$\underline{\underline{C}}(t, t')$	$\begin{pmatrix} 1 & -\gamma & 0 \\ -\gamma & 1 + \gamma^2 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{\epsilon} & 0 & 0 \\ 0 & e^{\epsilon} & 0 \\ 0 & 0 & e^{-2\epsilon} \end{pmatrix}_{123}$	$\underline{\underline{I}}$
$\underline{\underline{C}}^{-1}(t', t)$	$\begin{pmatrix} 1 + \gamma^2 & \gamma & 0 \\ \gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{-\epsilon} & 0 & 0 \\ 0 & e^{-\epsilon} & 0 \\ 0 & 0 & e^{2\epsilon} \end{pmatrix}_{123}$	$\underline{\underline{I}}$
$\underline{\underline{\gamma}}^{[ol]}(t, t')$	$\begin{pmatrix} 0 & -\gamma & 0 \\ -\gamma & \gamma^2 & 0 \\ 0 & 0 & 1 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{\epsilon} - 1 & 0 & 0 \\ 0 & e^{\epsilon} - 1 & 0 \\ 0 & 0 & e^{-2\epsilon} - 1 \end{pmatrix}_{123}$	$\underline{\underline{0}}$
$\underline{\underline{\gamma}}_{[ol]}(t, t')$	$\begin{pmatrix} -\gamma^2 & \gamma & 0 \\ \gamma & 0 & 0 \\ 0 & 0 & 0 \end{pmatrix}_{123}$	$\begin{pmatrix} e^{-\epsilon} - 1 & 0 & 0 \\ 0 & e^{-\epsilon} - 1 & 0 \\ 0 & 0 & e^{2\epsilon} - 1 \end{pmatrix}_{123}$	$\underline{\underline{0}}$

Table 9.3: Strain tensors for shear and extension in Cartesian coordinates.

For shear flows $\gamma = \gamma(t', t) = \int_{t'}^t \dot{\zeta}(t'') dt'' = \int_{t'}^t \dot{\gamma}_{21}(t'') dt''$ and for elongational flows

$\epsilon = \epsilon(t', t) = \int_{t'}^t \dot{\epsilon}(t'') dt''$. The angle ψ is the angle from $\underline{r}(t) = \underline{r}$ to $\underline{r}(t') = \underline{r}'$ in counter-

clockwise (ccw) rotation around the \hat{e}_3 -axis.

We desire a strain tensor that accurately captures large-strain deformation without being affected by rigid-body rotation.

$$\left. \begin{array}{l} \nabla \underline{u} \\ \underline{\gamma} \\ \underline{\underline{F}} \\ \underline{\underline{F}}^{-1} \end{array} \right\}$$

All these strain measures include both deformation and orientation

We can separate the deformation and orientation information in $\underline{\underline{F}}$ and $\underline{\underline{F}}^{-1}$ using a technique called *polar decomposition*.

© Faith A. Morrison, Michigan

Solve for x', y', z' as a function of x, y, z

$$x' = x - (t-t') \dot{\gamma}_0 y$$

$$y' = y$$

$$z' = z$$

Now, carry out derivations in \underline{E}

$$\underline{F} = \begin{pmatrix} 1 & 0 & 0 \\ -(t-t') \dot{\gamma}_0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{matrix} x \\ y \\ z \end{matrix}$$

$$\text{let } \gamma = \int_{t'}^t \dot{\gamma}_0 dt'' = \dot{\gamma}_0 (t-t')$$

$$\underline{F} = \begin{pmatrix} 1 & 0 & 0 \\ -\gamma & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix} \begin{matrix} x \\ y \\ z \end{matrix}$$

Polar Decomposition Theorem

Any tensor for which an inverse exists has two unique decompositions:

$$\begin{aligned} \underline{\underline{A}} &= \underline{\underline{R}} \cdot \underline{\underline{U}} \\ &= \underline{\underline{V}} \cdot \underline{\underline{R}} \end{aligned}$$

Pure rotation tensor

$$\underline{\underline{U}} = \left(\underline{\underline{A}}^T \cdot \underline{\underline{A}} \right)^{\frac{1}{2}}$$

$$\underline{\underline{V}} = \left(\underline{\underline{A}} \cdot \underline{\underline{A}}^T \right)^{\frac{1}{2}}$$

$$\underline{\underline{R}} = \underline{\underline{A}} \cdot \left(\underline{\underline{A}}^T \cdot \underline{\underline{A}} \right)^{-\frac{1}{2}} = \underline{\underline{A}} \cdot \underline{\underline{U}}^{-1}$$

$$\underline{\underline{R}}^{-1} = \underline{\underline{R}}^T$$

Orthogonal tensor

$$\underline{\underline{U}}, \underline{\underline{V}}$$

Symmetric, nonsingular tensors

© Faith A. Morrison, Michigan

36-2

9.5

$$\underline{R}^T = \underline{R}^{-1}$$

Consider an arbitrary vector \underline{v}

$$\underline{R} \cdot \underline{v} = \underline{w}$$

NOTE: $\underline{w} =$ ~~\underline{v}~~ $(\underline{R} \cdot \underline{v}) = \underline{v} \cdot \underline{R}^T$

verify w)
Einstein
notation

calculate $|\underline{w}|$

$$\sqrt{\underline{w} \cdot \underline{w}} = (\underline{R} \cdot \underline{v} \cdot \underline{R} \cdot \underline{v})^{\frac{1}{2}}$$

$$= (\underline{v} \cdot \underline{R}^T \cdot \underline{R} \cdot \underline{v})^{\frac{1}{2}}$$

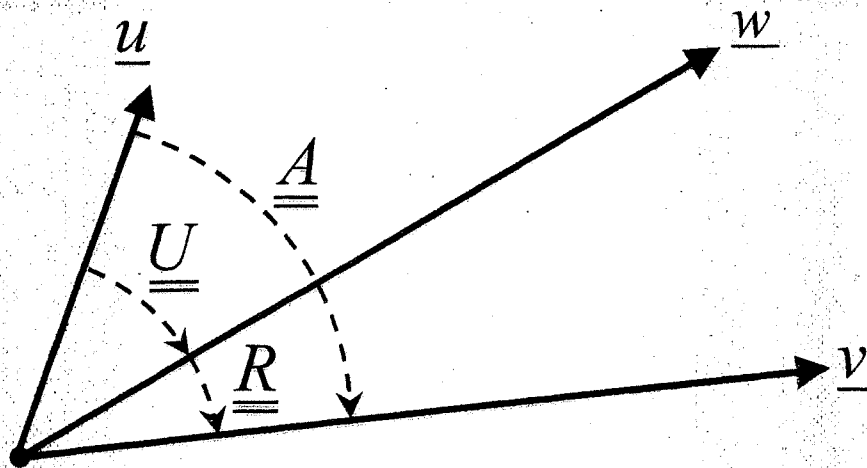
$$= \underline{I}$$

$$(\underline{v} \cdot \underline{v})^{\frac{1}{2}} = |\underline{v}|$$

$$= |\underline{v}|$$

EXAMPLE: Calculate the right stretch tensor and rotation tensor for a given tensor. Calculate the angle through which $\underline{\underline{R}}$ rotates the vector \underline{u} .

$$\underline{\underline{A}} = \begin{pmatrix} 1 & 0 & 2 \\ 0 & 3 & 2 \\ 2 & 0 & 0 \end{pmatrix}_{xyz} \quad \underline{u} = \begin{pmatrix} 1 \\ 2 \\ 1 \end{pmatrix}_{xyz}$$



© Faith A. Morrison, Michigan

(10)

24 13

We have partially isolated the effect of rotation through polar decomposition.

$$\underline{\underline{A}} = \underline{\underline{R}} \cdot \underline{\underline{U}} = \underline{\underline{V}} \cdot \underline{\underline{R}}$$

rotation tensor

left stretch tensor

original (strain) tensor

right stretch tensor

The diagram shows the polar decomposition equation $\underline{\underline{A}} = \underline{\underline{R}} \cdot \underline{\underline{U}} = \underline{\underline{V}} \cdot \underline{\underline{R}}$. A large arrow on the left points from the text 'original (strain) tensor' to the tensor $\underline{\underline{A}}$. An arrow points from 'rotation tensor' to $\underline{\underline{R}}$ in the first product. Another arrow points from 'left stretch tensor' to $\underline{\underline{U}}$ in the first product. A third arrow points from 'right stretch tensor' to $\underline{\underline{V}}$ in the second product.

We can further isolate stretch from rotation by considering the *eigenvectors* of $\underline{\underline{U}}$ and $\underline{\underline{V}}$.