

Exam 1 Formulas

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Rate of deformation tensor: $\underline{\dot{\gamma}} = \nabla \underline{v} + (\nabla \underline{v})^T$

Rate of deformation: $\dot{\gamma} = |\underline{\dot{\gamma}}|$

Tensor magnitude: $A = |\underline{A}| = \sqrt{\frac{\underline{A}:\underline{A}}{2}}$

Total stress tensor: $\underline{\Pi} = p\underline{I} + \underline{\tau}$
(Bird sign convention on stress)

Navier-Stokes Equation: $\rho \left(\frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \nabla \underline{v} \right) = -\nabla p + \mu \nabla^2 \underline{v} + \rho \underline{g}$

Cauchy Momentum Equation: $\rho \left(\frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \nabla \underline{v} \right) = -\nabla p - \nabla \cdot \underline{\tau} + \rho \underline{g}$
(Bird sign convention on stress)

Continuity Equation: $\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \underline{v})$

Newtonian, incompressible constitutive equation: $\underline{\tau} = -\mu(\nabla \underline{v} + (\nabla \underline{v})^T)$
(Bird sign convention on stress)

Fluid force \underline{F}_{on} on a surface S:
(Bird sign convention on stress)

$$\underline{F}_{on} = \iint_S [\hat{n} \cdot -\underline{\Pi}]_{surface} dS$$

Flow rate Q through a surface S:

$$Q = \iint_S [\hat{n} \cdot \underline{v}]_{surface} dS$$

Fluid torque \underline{T}_{on} on a surface S: ($\underline{\tilde{R}}$ is the lever arm vector from the axis of rotation to the point of application of the force)
(Bird sign convention on stress)

$$\underline{T}_{on} = \iint_S [\underline{\tilde{R}} \times (\hat{n} \cdot -\underline{\Pi})]_{surface} dS$$

Table of Integrals

$$\int u^n du = \frac{u^{n+1}}{n+1} + C, n \text{ is a constant}$$

$$\int \frac{1}{y} du = \ln u + C$$

$$\int \ln u du = u \ln u - u + C$$

$$\int_a^b u dv = uv \Big|_a^b - \int_a^b v du$$

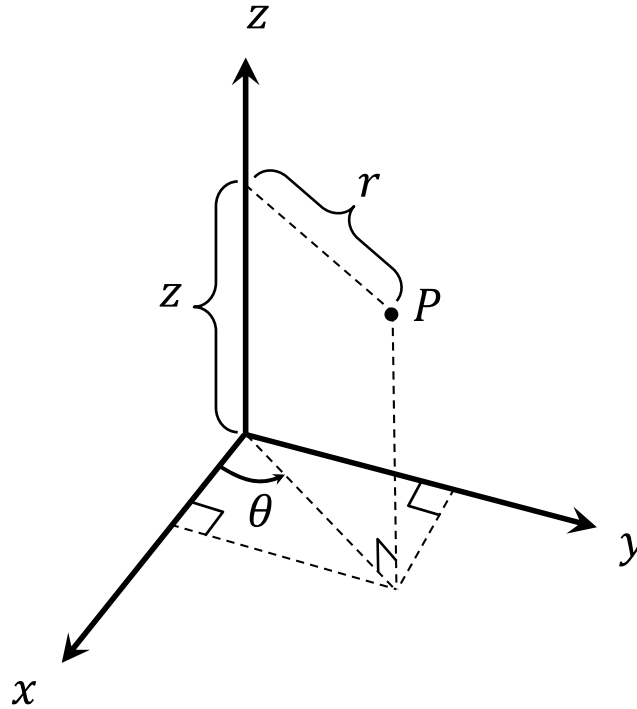
Miscellaneous

$$\underline{\underline{A}} = \begin{pmatrix} A_{11} & A_{12} & A_{13} \\ A_{21} & A_{22} & A_{23} \\ A_{31} & A_{32} & A_{33} \end{pmatrix}_{123}$$

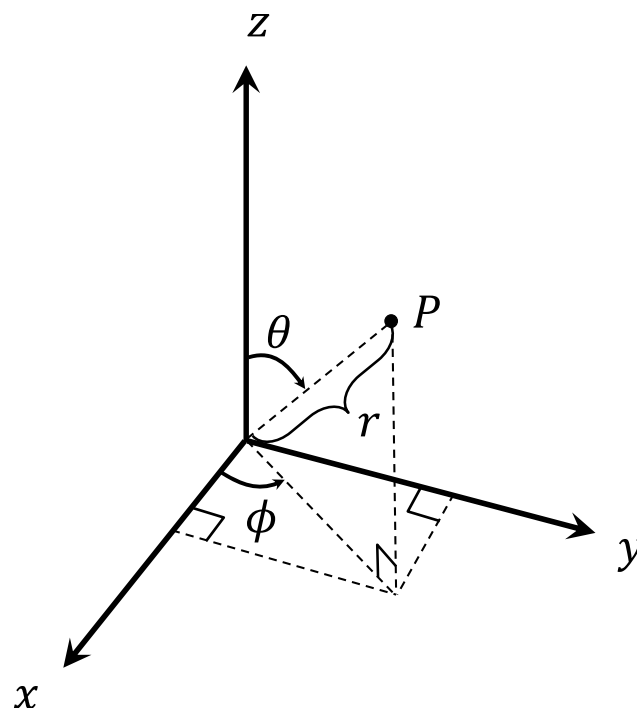
$$\frac{d}{ds}(uw) = u \frac{dw}{ds} + w \frac{du}{ds}$$

$$\underline{u} \times \underline{w} = \det \begin{vmatrix} \hat{e}_1 & \hat{e}_2 & \hat{e}_3 \\ u_1 & u_2 & u_3 \\ w_1 & w_2 & w_3 \end{vmatrix} = \begin{pmatrix} u_2 w_3 - u_3 w_2 \\ -(u_1 w_3 - u_3 w_1) \\ u_1 w_2 - u_2 w_1 \end{pmatrix}_{123}$$

Cylindrical Coordinate System: Note that the θ -coordinate swings around the z -axis and the r -coordinate is perpendicular to the z -axis.



Spherical Coordinate System: Note that the θ -coordinate swings down from the z -axis and the r -coordinate emits radially from the origin; these are different from their definitions in the cylindrical system above.



System	Coordinates	Basis vectors
Spherical	$x = r \sin \theta \cos \phi$	$\hat{e}_r = (\sin \theta \cos \phi)\hat{e}_x + (\sin \theta \sin \phi)\hat{e}_y + \cos \theta \hat{e}_z$
Spherical	$y = r \sin \theta \sin \phi$	$\hat{e}_\theta = (\cos \theta \cos \phi)\hat{e}_x + (\cos \theta \sin \phi)\hat{e}_y + (-\sin \theta)\hat{e}_z$
Spherical	$z = r \cos \theta$	$\hat{e}_\phi = (-\sin \phi)\hat{e}_x + \cos \phi \hat{e}_y$
Cylindrical	$x = r \cos \theta$	$\hat{e}_r = \cos \theta \hat{e}_x + \sin \theta \hat{e}_y$
Cylindrical	$y = r \sin \theta$	$\hat{e}_\theta = (-\sin \theta)\hat{e}_x + \cos \theta \hat{e}_y$
Cylindrical	$z = z$	$\hat{e}_z = \hat{e}_z$

Coordinate system	surface differential dS
Cartesian (top, $\hat{n} = \hat{e}_z$)	$dS = dx dy$
Cartesian (side a, $\hat{n} = \hat{e}_y$)	$dS = dx dz$
Cartesian (side b, $\hat{n} = \hat{e}_x$)	$dS = dy dz$
cylindrical (top, $\hat{n} = \hat{e}_z$)	$dS = r dr d\theta$
cylindrical (side, $\hat{n} = \hat{e}_r$)	$dS = R d\theta dz$
spherical, ($\hat{n} = \hat{e}_r$)	$dS = R^2 \sin \theta d\theta d\phi$

Coordinate system	volume differential dV
Cartesian	$dV = dx dy dz$
cylindrical	$dV = r dr d\theta dz$
spherical	$dV = r^2 \sin \theta dr d\theta d\phi$