

Exam 2 Formulas

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Rate of deformation tensor: $\underline{\dot{\gamma}} = \nabla \underline{v} + (\nabla \underline{v})^T$

Rate of deformation: $\dot{\gamma} = |\underline{\dot{\gamma}}|$

Tensor magnitude: $A = |\underline{A}| = \sqrt{\frac{A:A}{2}}$

Shear strain: $\gamma_{21}(t_a, t_b) = \int_{t_a}^{t_b} \dot{\gamma}_{21}(t'') dt''$

Navier-Stokes Equation: $\rho \left(\frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \nabla \underline{v} \right) = -\nabla p + \mu \nabla^2 \underline{v} + \rho \underline{g}$

Cauchy Momentum Equation: $\rho \left(\frac{\partial \underline{v}}{\partial t} + \underline{v} \cdot \nabla \underline{v} \right) = -\nabla p - \nabla \cdot \underline{\tau} + \rho \underline{g}$

Continuity Equation: $\frac{\partial \rho}{\partial t} = -\nabla \cdot (\rho \underline{v})$

Fluid force \underline{F} on a surface S:

$$\underline{F} = \iint_S [\hat{\mathbf{n}} \cdot -\underline{\Pi}]_{surface} dA$$

Flow rate Q through a surface S:

$$Q = \iint_S [\hat{\mathbf{n}} \cdot \underline{v}]_{surface} dA$$

Fluid torque \underline{T} on a surface S: (\underline{R} is the vector from the axis of rotation to the point of application of the force)

$$\underline{T} = \iint_S [\underline{R} \times (\hat{\mathbf{n}} \cdot -\underline{\Pi})]_{surface} dA$$

Newtonian, incompressible fluid: $\underline{\boldsymbol{\tau}} = -\boldsymbol{\mu}(\nabla\underline{\boldsymbol{v}} + (\nabla\underline{\boldsymbol{v}})^T)$

Generalized Newtonian fluid (GNF): $\underline{\boldsymbol{\tau}} = -\boldsymbol{\eta}(\dot{\boldsymbol{\gamma}})\dot{\boldsymbol{\gamma}}$

Power-law GNF model: $\boldsymbol{\eta}(\dot{\boldsymbol{\gamma}}) = m\dot{\boldsymbol{\gamma}}^{n-1}$

(Note that m and n are parameters of the model and are constants)

Carreau-Yasuda GNF model: $\boldsymbol{\eta}(\dot{\boldsymbol{\gamma}}) = \boldsymbol{\eta}_\infty + (\boldsymbol{\eta}_0 - \boldsymbol{\eta}_\infty)[\mathbf{1} + (\dot{\boldsymbol{\gamma}}\boldsymbol{\lambda})^a]^{\frac{n-1}{a}}$

(Note that a , $\boldsymbol{\lambda}$ and n , $\boldsymbol{\eta}_0$, and $\boldsymbol{\eta}_\infty$ are parameters of the model and are constants)

Elongational flow (uniaxial, biaxial): $\underline{\boldsymbol{v}} = \begin{pmatrix} -\frac{\dot{\boldsymbol{\epsilon}}(t)}{2}\boldsymbol{x}_1 \\ -\frac{\dot{\boldsymbol{\epsilon}}(t)}{2}\boldsymbol{x}_2 \\ \dot{\boldsymbol{\epsilon}}(t)\boldsymbol{x}_3 \end{pmatrix}_{123}$

Shear flow: $\underline{\boldsymbol{v}} = \begin{pmatrix} \dot{\boldsymbol{\zeta}}(t)\boldsymbol{x}_2 \\ \mathbf{0} \\ \mathbf{0} \end{pmatrix}_{123}$

Steady shearing kinematics: $\dot{\boldsymbol{\zeta}}(t) = \dot{\boldsymbol{\gamma}}_0$ for all values of time t

Start-up of steady shearing kinematics: $\dot{\boldsymbol{\zeta}}(t) = \begin{cases} \mathbf{0} & t < 0 \\ \dot{\boldsymbol{\gamma}}_0 & t \geq 0 \end{cases}$

Cessation of steady shearing kinematics: $\dot{\boldsymbol{\zeta}}(t) = \begin{cases} \dot{\boldsymbol{\gamma}}_0 & t < 0 \\ \mathbf{0} & t \geq 0 \end{cases}$

Steady elongational kinematics: $\dot{\boldsymbol{\epsilon}}(t) = \dot{\boldsymbol{\epsilon}}_0$

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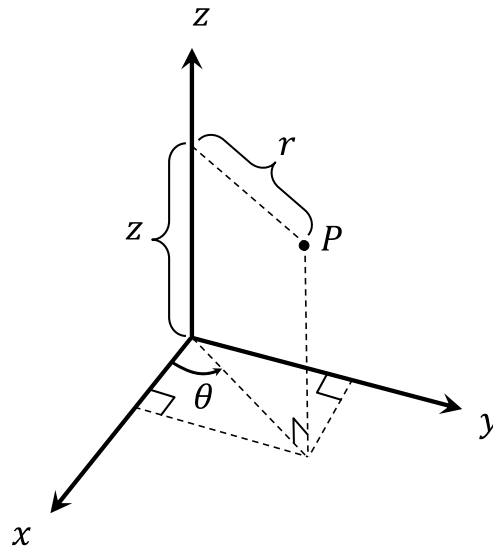
Cessation of steady elongation kinematics: $\dot{\boldsymbol{\epsilon}}(t) = \begin{cases} \dot{\boldsymbol{\epsilon}}_0 & t < 0 \\ \mathbf{0} & t \geq 0 \end{cases}$

Shear viscosity: $\boldsymbol{\eta} = \frac{-(\boldsymbol{\tau}_{21})}{\dot{\boldsymbol{\gamma}}_0}$

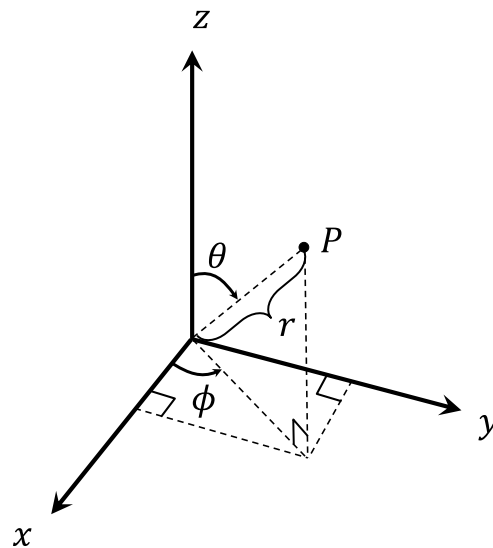
Shear normal stress coefficients: $\boldsymbol{\Psi}_1 = \frac{-(\boldsymbol{\tau}_{11}-\boldsymbol{\tau}_{22})}{\dot{\boldsymbol{\gamma}}_0^2}$, $\boldsymbol{\Psi}_2 = \frac{-(\boldsymbol{\tau}_{22}-\boldsymbol{\tau}_{33})}{\dot{\boldsymbol{\gamma}}_0}$

Elongational viscosity: $\bar{\boldsymbol{\eta}} = \frac{-(\boldsymbol{\tau}_{33}-\boldsymbol{\tau}_{11})}{\dot{\boldsymbol{\epsilon}}_0}$

Cylindrical Coordinate System: Note that the θ -coordinate swings around the z -axis and the r -coordinate is perpendicular to the z -axis.



Spherical Coordinate System: Note that the θ -coordinate swings down from the z -axis and the r -coordinate emits radially from the origin; these are different from their definitions in the cylindrical system above.



System	Coordinates	Basis vectors
Spherical	$x = r \sin \theta \cos \phi$	$\hat{e}_r = (\sin \theta \cos \phi) \hat{e}_x + (\sin \theta \sin \phi) \hat{e}_y + \cos \theta \hat{e}_z$
Spherical	$y = r \sin \theta \sin \phi$	$\hat{e}_\theta = (\cos \theta \cos \phi) \hat{e}_x + (\cos \theta \sin \phi) \hat{e}_y + (-\sin \theta) \hat{e}_z$
Spherical	$z = r \cos \theta$	$\hat{e}_\phi = (-\sin \phi) \hat{e}_x + \cos \phi \hat{e}_y$
Cylindrical	$x = r \cos \theta$	$\hat{e}_r = \cos \theta \hat{e}_x + \sin \theta \hat{e}_y$
Cylindrical	$y = r \sin \theta$	$\hat{e}_\theta = (-\sin \theta) \hat{e}_x + \cos \theta \hat{e}_y$
Cylindrical	$z = z$	$\hat{e}_z = \hat{e}_z$