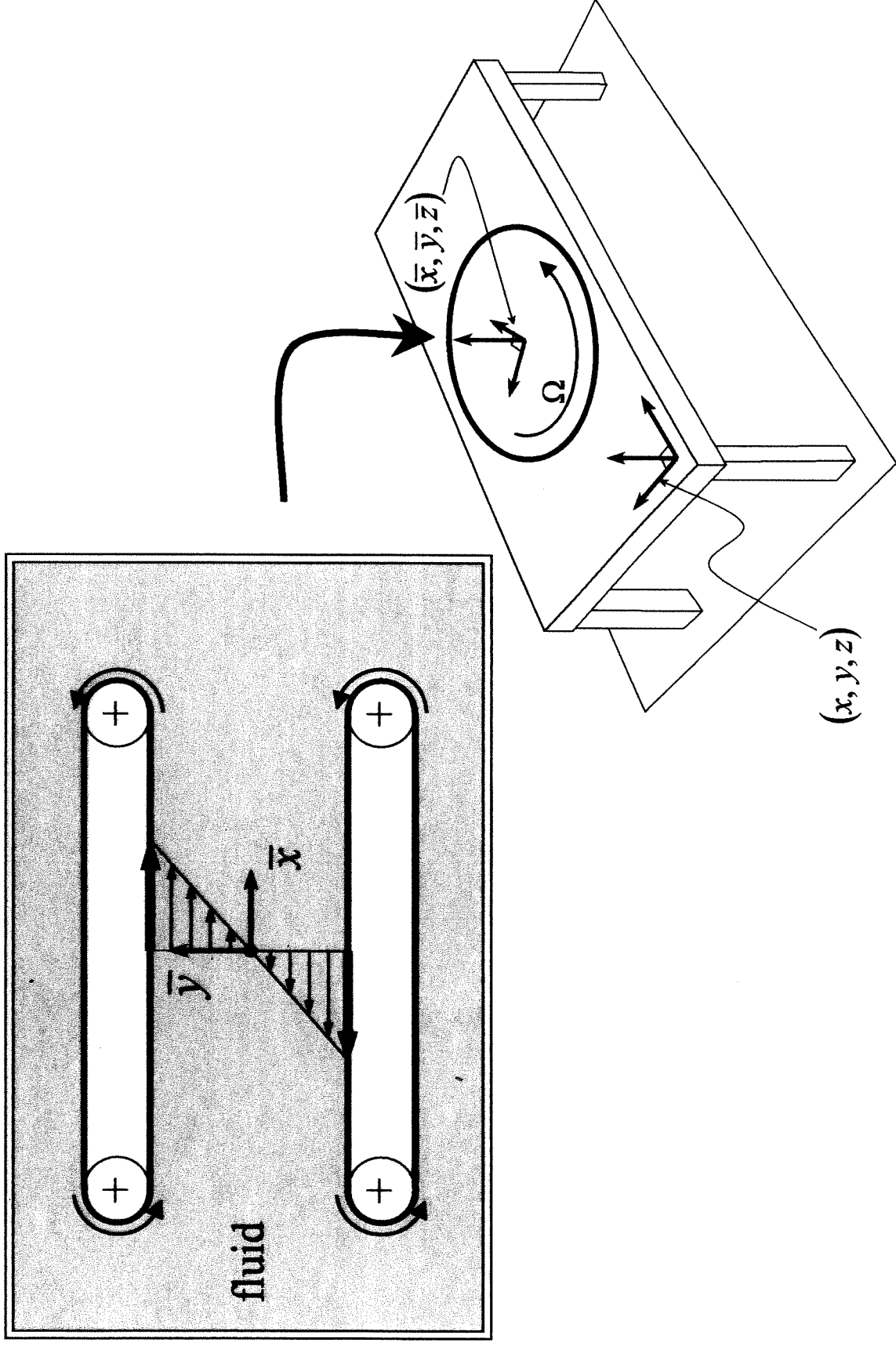


# Shear flow in a rotating frame of reference

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Shear flow from the different viewpoints of two observers:

- ① one rotating with flow
- ② one stationary

Both should give the same prediction for viscosity

$\bar{x}, \bar{y}, \bar{z}$  rotating, shear coordinate system

$x, y, z$  stationary, non shear coord system  
(except when  $t=0$ )

Strategy: Calculate  $\eta$  predicted by GLE model using both points of view

PART I: (easy) Calc  $\underline{x}$  in  $\bar{x}, \bar{y}, \bar{z}$  systems

$$\underline{v} = \begin{pmatrix} \dot{x}_0 \dot{y}_0 \\ 0 \\ 0 \end{pmatrix} \bar{x} \bar{y} \bar{z} \quad \dot{\underline{x}} = \begin{pmatrix} 0 \dot{x}_0 \dot{y}_0 \\ \dot{x}_0 \dot{y}_0 \\ 0 \dot{y}_0 \end{pmatrix} \bar{x} \bar{y} \bar{z}$$

Now calculate  $\underline{\ddot{x}}$  using GLE:

$$\underline{\ddot{x}} = - \int_{-\infty}^t G(t-\tau) \dot{\underline{x}}(\tau) d\tau$$

$$= - \int_{-\infty}^t G(t-\tau) \begin{pmatrix} 0 \dot{x}_0 \dot{y}_0 \\ \dot{x}_0 \dot{y}_0 \\ 0 \dot{y}_0 \end{pmatrix} \bar{x} \bar{y} \bar{z} d\tau$$

defn of material function  $\eta$ :

$$\eta \equiv -\frac{\tau_{23}}{\dot{\gamma}_0} = \frac{1}{\dot{\gamma}_0} \int_{-\infty}^t G(t-t') \dot{\gamma}_0 dt'$$

$$s = t - t'$$

$$ds = -dt'$$

$$t' = -\infty \quad s = \infty$$

$$t' = t \quad s = 0$$

$$\eta = \int_0^{\infty} G(s) ds$$

This is what we have always gotten in this calculation.

Now, carry out the same calculation in the stationary coord system ... (HARDER)

(4)

What is the velocity of fluid particles written with respect to a stationary observer?

$$\underline{U}_{\text{wrt stationary frame}} = \underline{U}_{\text{wrt rotating frame}} + \underline{U}_{\text{frame}}$$

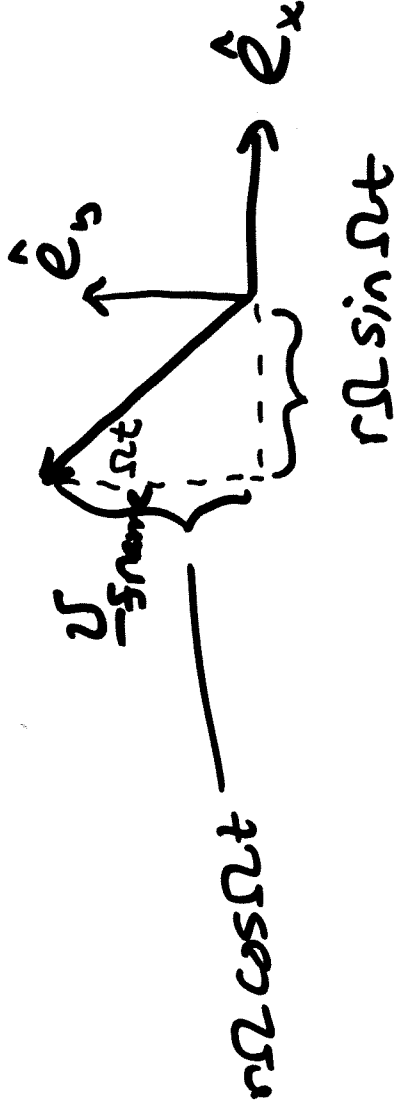
$$= \delta_0 \bar{y} \hat{e}_{\bar{x}} + \underline{U}_{\text{frame}}$$

need to write these wrt stationary frame

need to figure out what this is

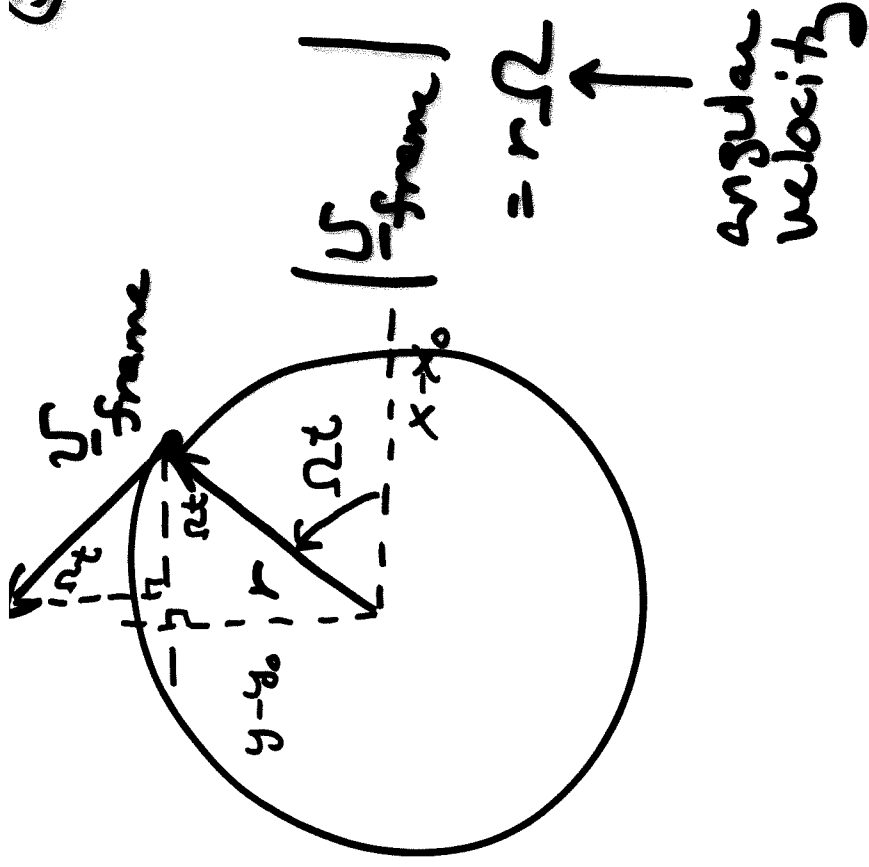
What is  $\underline{v}_{\text{frame}}$  ?

The velocity of any point on the turntable written in the stationary frame is  $r\Omega$  pointing in a tangent direction.

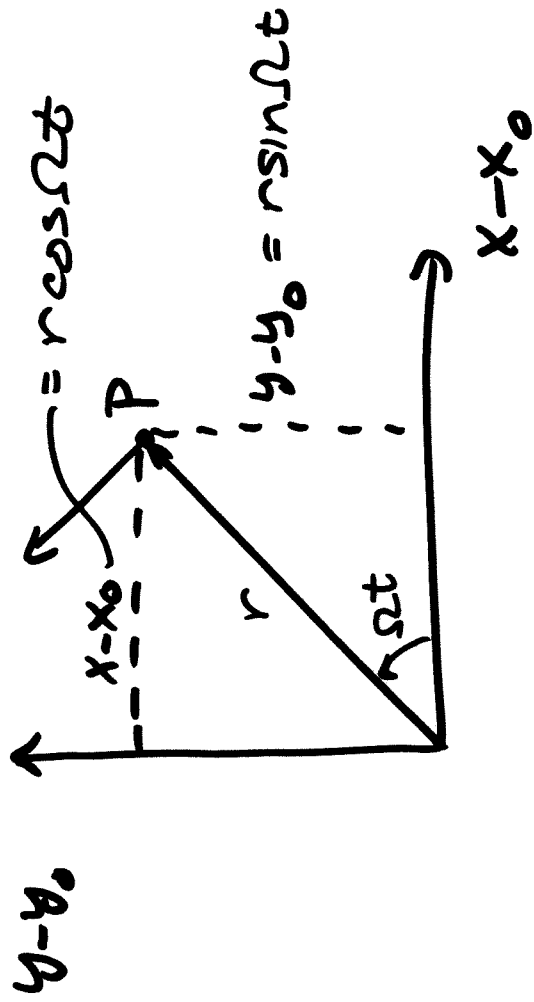


$$\underline{v}_{\text{frame}} = -r\Omega \sin \Omega t \hat{e}_x + r\Omega \cos \Omega t \hat{e}_y$$

(5)



(5)



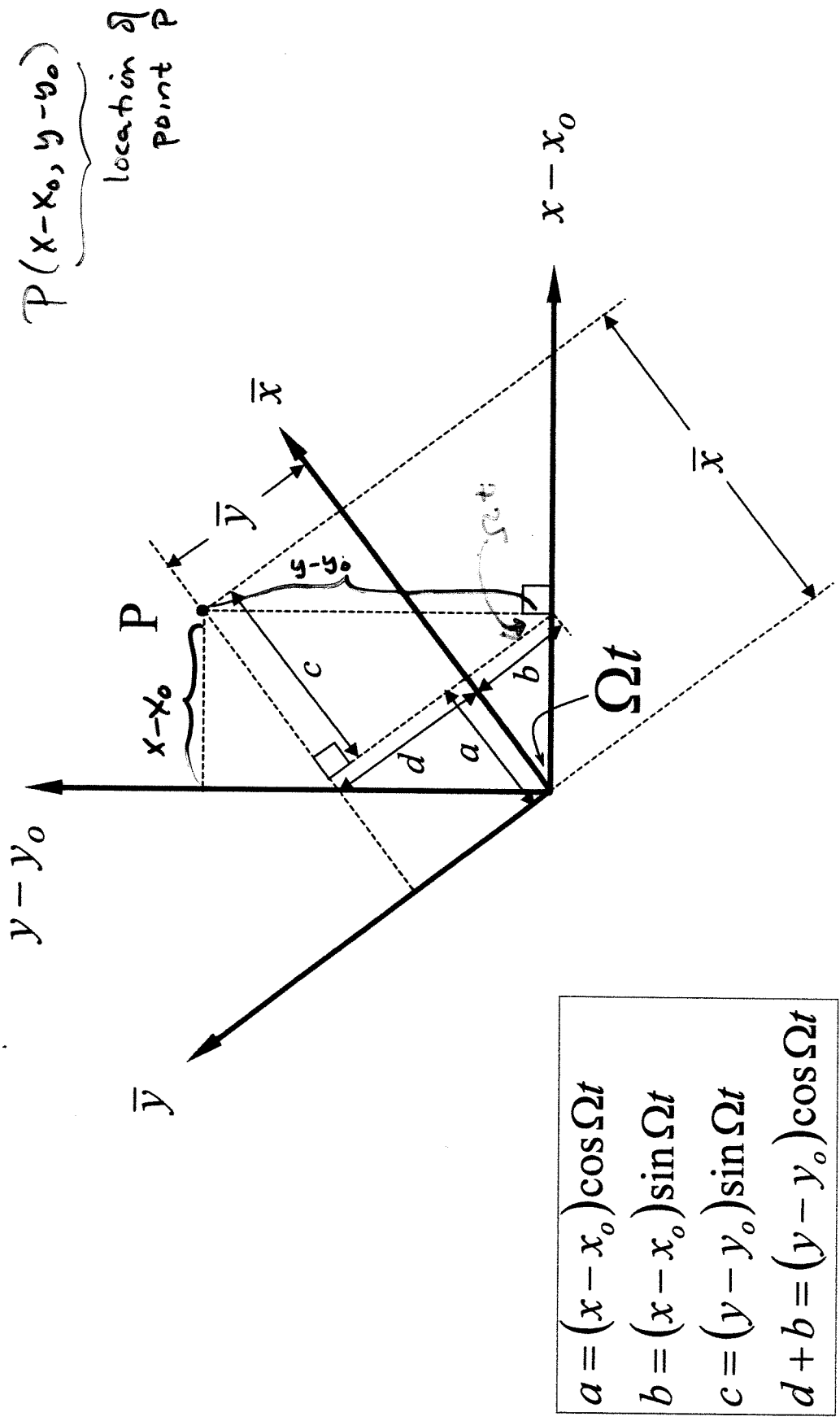
Point P:  
 $(x-x_0, y-y_0)$

$$\underline{v}_{\text{frame}} = -\Omega \left( \frac{r \sin \Omega t}{y-y_0} \right) \hat{e}_x + \Omega \left( \frac{r \cos \Omega t}{x-x_0} \right) \hat{e}_y$$

$$\underline{v}_{\text{frame}} = -\Omega (y-y_0) \hat{e}_x + \Omega (x-x_0) \hat{e}_y$$

The next step is the coordinate transformation of the fluid velocity....

# Shear flow in a rotating frame of reference





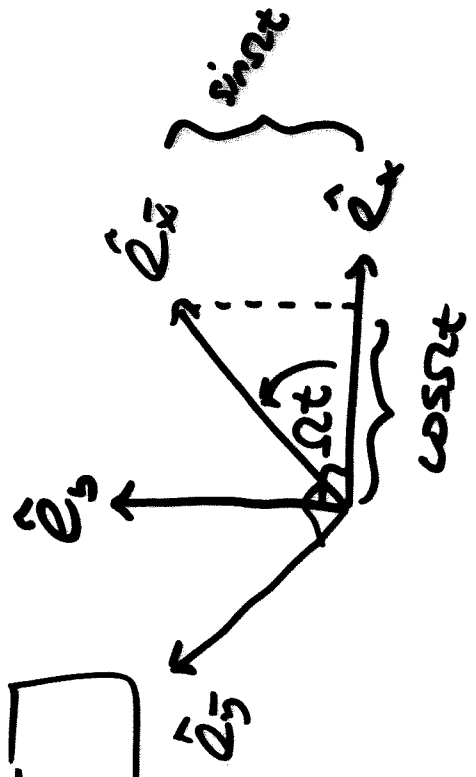
$\dot{\bar{y}} \bar{e}_{\bar{x}}$

what is  $\hat{e}_{\bar{x}}$  in terms of  $\hat{e}_x, \hat{e}_y$ ?  
what is  $\bar{y}$  in terms of  $x-x_0, y-y_0$ ?

$$\bar{y} = d = (y-y_0) \cos \Omega t - b \overset{(x-x_0) \sin \Omega t}{\leftarrow}$$

$$\bar{y} = (y-y_0) \cos \Omega t - (x-x_0) \sin \Omega t$$

$$\hat{e}_{\bar{x}} = \cos \Omega t \hat{e}_x + \sin \Omega t \hat{e}_y$$



Now, Assemble ...

$$\underline{V}_{\text{stationary frame}} = \dot{\delta}_0 \bar{y} \hat{e}_x + \underline{V}_{\text{frame}}$$

$$= \dot{\delta}_0 \left[ (y-y_0) \cos \Omega t - (x-x_0) \sin \Omega t \right] \\ \left[ \cos \Omega t \hat{e}_x + \sin \Omega t \hat{e}_y \right] \\ + \left[ -\Omega (y-y_0) \hat{e}_x + \Omega (x-x_0) \hat{e}_y \right]$$

$$= \begin{pmatrix} \dot{\delta}_0 \cos \Omega t \left[ (y-y_0) \cos \Omega t - (x-x_0) \sin \Omega t \right] \\ - \Omega (y-y_0) \\ \dot{\delta}_0 \sin \Omega t \left[ (y-y_0) \cos \Omega t - (x-x_0) \sin \Omega t \right] \\ + \Omega (x-x_0) \\ 0 \end{pmatrix} \begin{matrix} x \\ y \\ z \end{matrix}$$

We need  $\underline{\dot{\gamma}}$  for the constitutive eqn, from which we'll calculate  $\underline{\tau_{xy}}$  and  $\underline{\tau_{yz}}$ .

$$\underline{\dot{\gamma}} = \underline{D\underline{v}} + (\underline{D\underline{v}})^T$$

$$D\underline{v} = \begin{pmatrix} -\sin\Omega t \dot{\gamma}_0 \cos\Omega t & -\sin\Omega t \dot{\gamma}_0 \sin\Omega t + \Omega & 0 \\ \dot{\gamma}_0 \cos\Omega t - \Omega & \dot{\gamma}_0 \sin\Omega t \cos\Omega t & 0 \\ 0 & 0 & 0 \end{pmatrix}$$

eqn

(10)

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$$\dot{\delta} = \begin{pmatrix} \overbrace{-2 \sin \Omega t \cos \Omega t}^{\sin 2\Omega t} \dot{\delta}_0 & \overbrace{\dot{\delta}_0 (\cos^2 \Omega t - \sin^2 \Omega t)}^{\cos 2\Omega t} & 0 \\ \dot{\delta}_0 \cos^2 \Omega t - \sin^2 \Omega t & 2 \sin \Omega t \cos \Omega t & 0 \\ 0 & 0 & 0 \end{pmatrix} \delta$$

$$\ddot{\delta} = \begin{pmatrix} -(\sin^2 \Omega t) \dot{\delta}_0 & \dot{\delta}_0 \cos 2\Omega t & 0 \\ \dot{\delta}_0 \cos 2\Omega t & \dot{\delta}_0 \sin 2\Omega t & 0 \\ 0 & 0 & 0 \end{pmatrix} \delta$$

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Now, we predict  $\gamma$ :

$$\gamma = -\frac{\tau_{xy}}{\delta_0}$$

This definition is tied to the shear coordinate system 123, but xyz is not a shear coord system except when  $t=0$ .

$$\tau_{yx}(t) = - \int_{-\infty}^t G(t-t') \dot{\gamma}_{yx}(t') dt'$$

$$s = t - t'$$

$$ds = -dt'$$

$$t' = -\infty \quad s = \infty$$

$$t' = t \quad s = 0$$

$$\tau_{yx}(t) = - \int_0^{\infty} G(s) \dot{\gamma}_{yx}(t-s) ds$$

$$= - \int_0^{\infty} \dot{\gamma}_0 G(s) \cos(2\Omega(t-s)) ds$$

We can predict  $\eta$  only when  $t=0$

$$\text{at } t=0 \quad \eta_2 = \eta_1$$

$$\eta = \frac{-\eta_2}{\delta_0} = \frac{\int_0^{\infty} G(s) \cos(s) \cos(2s) ds}{\int_0^{\infty} G(s) ds}$$

$$\eta = \int_0^{\infty} G(s) \cos(s) ds$$

$$\eta = \int_0^{\infty} G(s) \cos(2s) ds$$

The predicted value of  $\eta$  depends on  $\Omega$ !!

Rotating Frame:  $\eta = \int_0^{\infty} G(s) ds$

Stationary Frame:  $\eta = \int_0^{\infty} G(s) \cos 2\Omega s ds$  X

\* PROBLEMS:

- ① should be the same
- ② should not depend on  $\Omega$

This is incorrect.

This shows that  
the GUVÉ eqn is  
not frame-invariant. //