



CM3110
Transport I
Part II: Heat Transfer



Michigan Tech



Heat Transfer with Phase Change
Evaporators and Condensers

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Heat Transfer with Phase Change

Heat Transfer with Phase Change

So far we have discussed heat transfer at a boundary due to convection in the fluid.

$$\left| \frac{q_x}{A} \right| = h |T_b - T_w|$$

Newton's law of cooling

1. forced convection
 - laminar
 - turbulent
2. natural convection

See also Incropera et al., *Fundamentals of Heat and Mass Transfer*, 6th edition, 2007, Chapter 10, *Boiling and Condensation*

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Heat Transfer with Phase Change

Heat Transfer with Phase Change

So far we have discussed heat transfer at a boundary due to convection in the fluid.

$$\left| \frac{q_x}{A} \right| = h |T_b - T_w|$$

Newton's law of cooling

1. forced convection
 - laminar
 - turbulent
2. natural convection
3. phase change

When a phase change takes place, the temperature on one side is **CONSTANT**, but the presence of boiling/condensing fluids produces heat transfer.

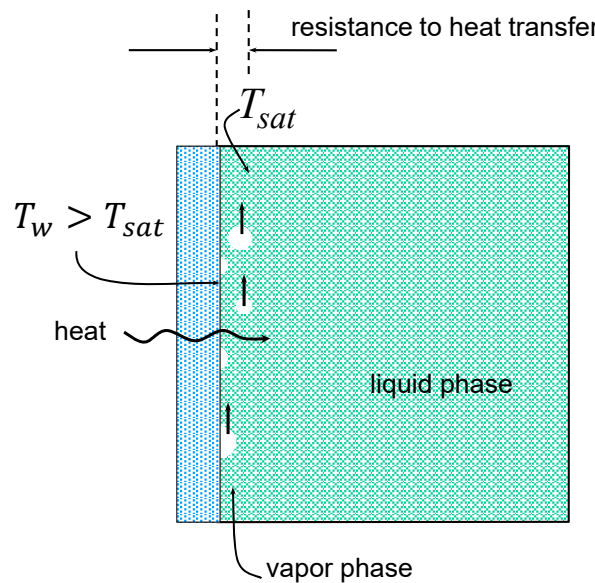
- Important in evaporation, distillation
- **LARGE h**
- It's important to know in which **regime** you operate
- Each regime has different correlations

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Heat Transfer with Phase Change

$$\Delta T = (T_w - T_{sat})$$

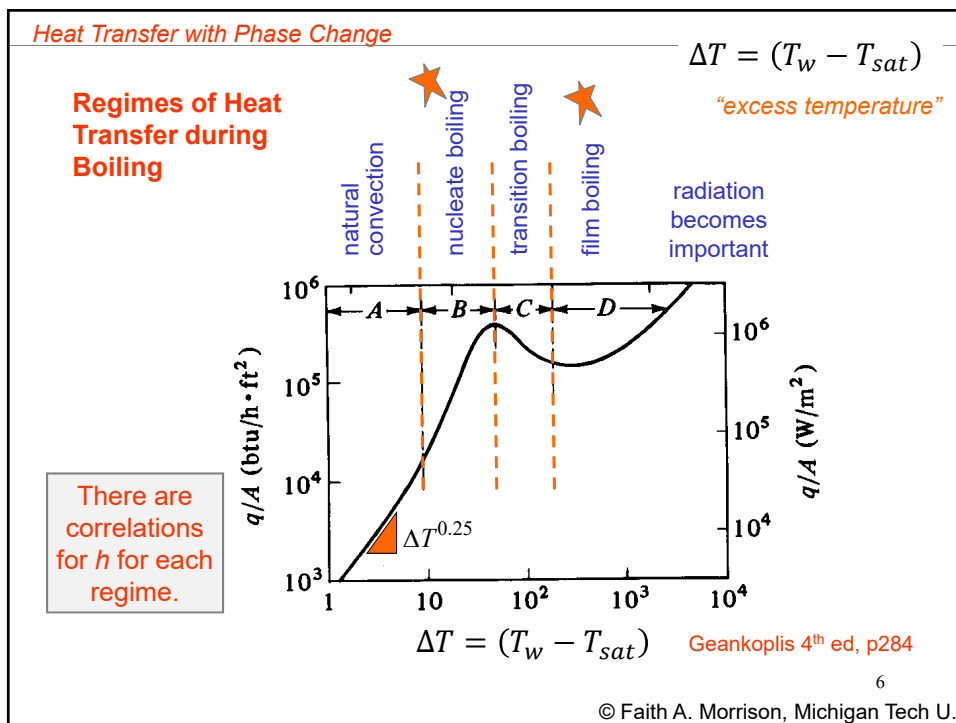
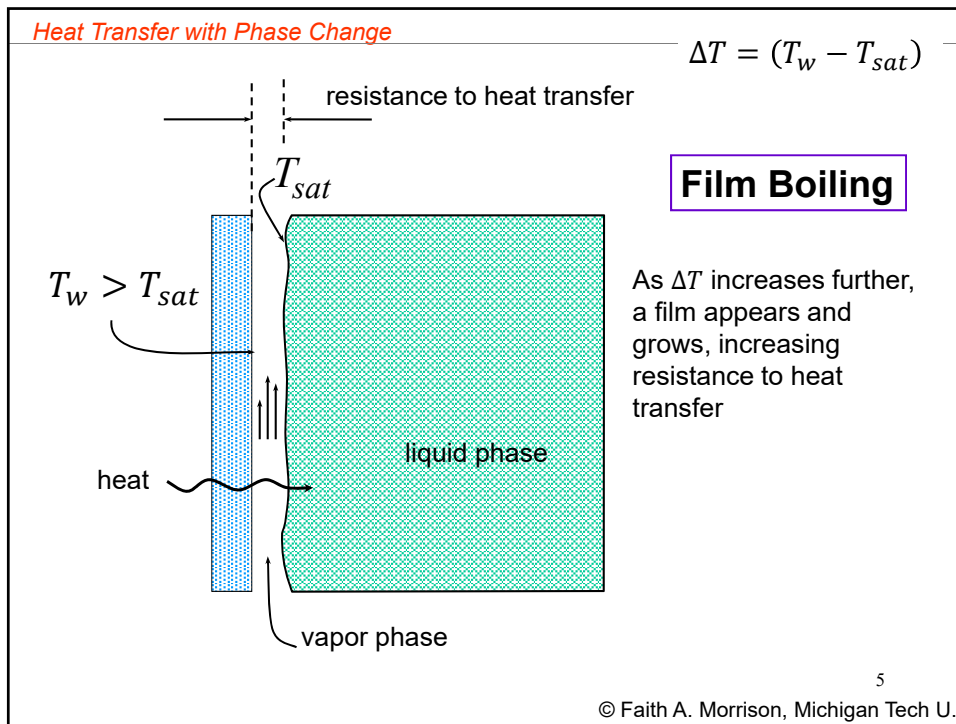
**Boiling**

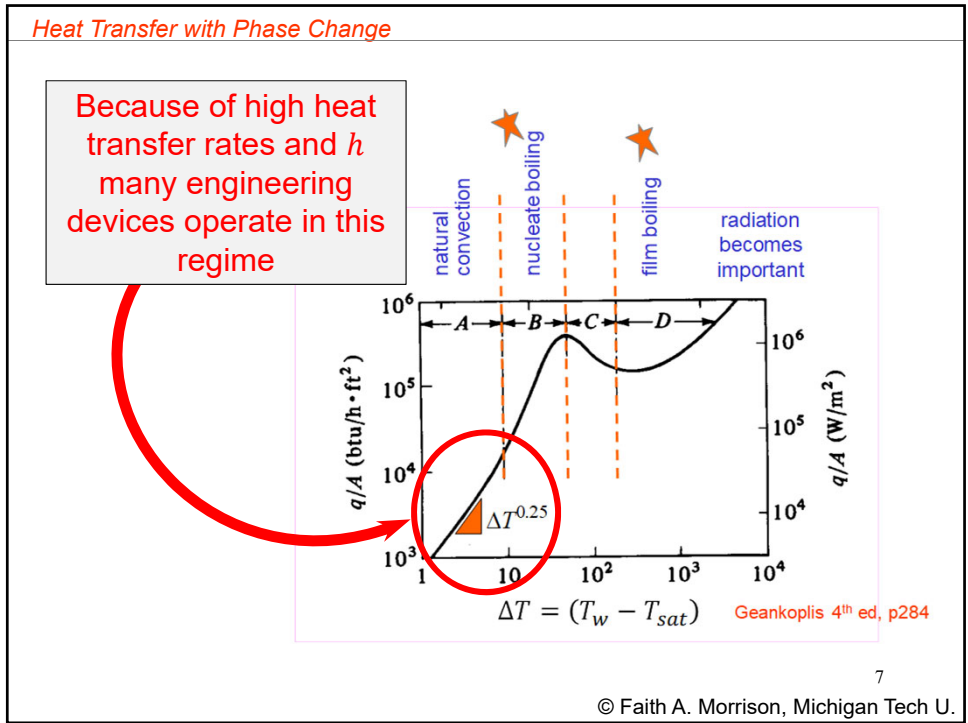
At low ΔT , few bubbles form, and heat transfer is by natural convection.

As ΔT increases, more bubbles form, increasing convection (flow) in the liquid phase, increasing h .

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Heat Transfer with Phase Change $\Delta T = (T_w - T_{sat})$

Regimes of Heat Transfer during Boiling

For example:
Nucleate boiling, horizontal surfaces

There are correlations for h for each regime.

$$h = 1043(\Delta T)^{\frac{1}{3}} \quad \frac{q}{A} < 16$$

$$h = 5.56(\Delta T)^3 \quad 16 < \frac{q}{A} < 240$$

Equations good for these units:

$$\Delta T [=] K$$

$$\frac{q}{A} [=] \frac{kW}{m^2}$$

$$h [=] \frac{W}{m^2 K}$$

Geankoplis 4th ed, p284

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Heat Transfer with Phase Change $\Delta T = (T_w - T_{sat})$

Regimes of Heat Transfer during Boiling There are correlations for h for each regime.

For example:
Nucleate boiling, vertical surfaces

$$h = 537(\Delta T)^{\frac{1}{7}} \quad \frac{q}{A} < 3$$

$$h = 7.95(\Delta T)^3 \quad 3 < \frac{q}{A} < 63$$

Equations good for these units:

$$\Delta T [=] K$$

$$\frac{q}{A} [=] \frac{kW}{m^2}$$

$$h [=] \frac{W}{m^2 K}$$

Geankoplis 4th ed, p285
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Heat Transfer with Phase Change $\Delta T = (T_w - T_{sat})$

Regimes of Heat Transfer during Boiling There are correlations for h for each regime.

For example:
Nucleate boiling, forced convection inside tubes

$$h = 2.55\Delta T^3 e^{\frac{p}{1551}}$$

Equations good for these units:

$$\Delta T [=] K$$

$$\frac{q}{A} [=] \frac{kW}{m^2}$$

$$h [=] \frac{W}{m^2 K}$$

$$p [=] kPa$$

Geankoplis 4th ed, p285
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Heat Transfer with Phase Change $\Delta T = (T_w - T_{sat})$

Regimes of Heat Transfer during Boiling

There are correlations for h for each regime.

For example:
Film boiling, horizontal tubes Geankoplis 4th ed, p285

$$h = 0.62 \left[\frac{(k_v^3 \rho_v (\rho_l - \rho_v) g [\Delta H(T_{sat}) + 0.4 \hat{C}_{p,v} \Delta T])}{D \mu_v \Delta T} \right]^{\frac{1}{4}}$$

Equations good for these units:

$\Delta T = (T_w - T_{sat}) [=] K$	$k_v [=] \frac{W}{mK}$	$\mu_v [=] Pa \cdot s$
$h [=] \frac{W}{m^2 K}$	$\rho_v, \rho_l [=] \frac{kg}{m^3}$	$g [=] m/s^2$
	$\Delta H [=] \frac{J}{kg}$	$T_{film} = \frac{T_{wall} + T_{sat}}{2}$
	$D [=] m$	(All material properties at the film temperature)

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Heat Transfer with Phase Change-Condensation $\Delta T = (T_{sat} - T_w)$

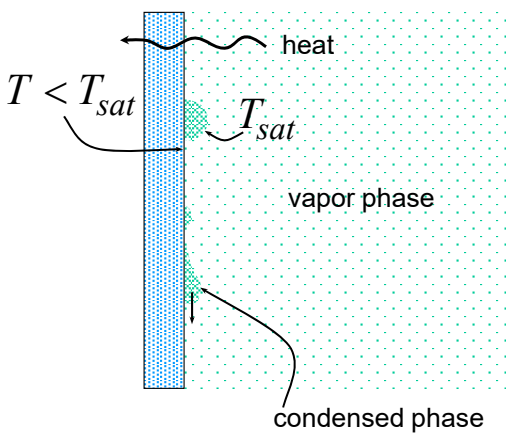
Condensation

At low ΔT , few droplets form,
 As ΔT increases, more droplets form, increasing convection (flow).
 Vertical plates;
 horizontal tubes important

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Heat Transfer with Phase Change-Condensation $\Delta T = (T_{sat} - T_w)$

Dropwise Condensation



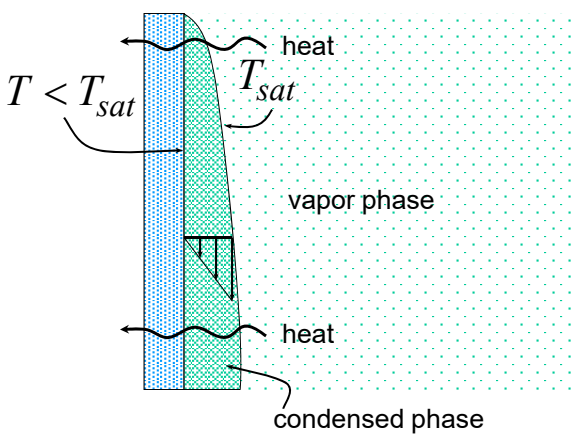
- high h
- hard to maintain
- not used in practice

There are correlations for h for each regime.

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Heat Transfer with Phase Change-Condensation $\Delta T = (T_{sat} - T_w)$

Film Condensation



- film reduces h
- very stable
- often used

There are correlations for h for each regime.

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Heat Transfer with Phase Change-Condensation

Regimes of Heat Transfer during Condensation

There are correlations for h for each regime.Geankoplis 4th ed, p289

For example:

Film condensation, vertical surfaces, laminar flow

$$Nu = \frac{hL}{k_l} = 1.13 \left(\frac{\rho_l(\rho_l - \rho_v)g\Delta H(T_{sat})L^3}{\mu_l k_l \Delta T} \right)^{\frac{1}{4}} \quad Re = \frac{4m}{\pi D \mu_l} < 1800$$

Equations good for these units:

$$\begin{array}{lll} \Delta T = (T_{sat} - T_w)[=]K & k_l [=] \frac{W}{mK} & \mu_l [=] Pa \cdot s \\ h [=] \frac{W}{m^2K} & \rho_v, \rho_l [=] \frac{kg}{m^3} & g [=] m/s^2 \\ m [=] \frac{kg}{s} & \Delta H [=] \frac{J}{kg} & T_{film} = \frac{T_{wall} + T_{sat}}{2} \\ & L [=] m & \end{array}$$

(All material properties at the film temperature)

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Heat Transfer with Phase Change-Condensation

Regimes of Heat Transfer during Condensation

There are correlations for h for each regime.Geankoplis 4th ed, p289

For example:

Film condensation, vertical surfaces, turbulent flow

$$Nu = \frac{hL}{k_l} = 0.0077 \left(\frac{\rho_l^2 g L^3}{\mu_l^2} \right)^{\frac{1}{3}} Re^{0.4} \quad Re = \frac{4m}{\pi D \mu_l} > 1800$$

Equations good for these units:

$$\begin{array}{lll} h [=] \frac{W}{m^2K} & \rho_l [=] \frac{kg}{m^3} & \mu_l [=] Pa \cdot s \\ m [=] \frac{kg}{s} & L [=] m & g [=] m/s^2 \\ & k_l [=] \frac{W}{m} & T_{film} = \frac{T_{wall} + T_{sat}}{2} \end{array}$$

(All material properties at the film temperature)

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Heat Transfer with Phase Change-Condensation $\Delta T = (T_{sat} - T_w)$

Regimes of Heat Transfer during Condensation There are correlations for h for each regime.

Geankoplis 4th ed, p285

For example:
Film condensation, outside horizontal cylinders, laminar flow

$$Nu = \frac{hL}{k_l} = 0.725 \left(\frac{\rho_l(\rho_l - \rho_v)g\Delta H(T_{sat})D^3}{N\mu_l k_l \Delta T} \right)^{\frac{1}{4}} \quad Re = \frac{4m}{\pi D \mu_l} < 1800$$

Equations good for these units:

$\Delta T = (T_{sat} - T_w) [=] K$	$k_l [=] \frac{W}{mK}$	$\mu_l [=] Pa \cdot s$
$h [=] \frac{W}{m^2K}$	$\rho_v, \rho_l [=] \frac{kg}{m^3}$	$g [=] m/s^2$
$m [=] \frac{kg}{s}$	$\Delta H [=] \frac{J}{kg}$	$T_{film} = \frac{T_{wall} + T_{sat}}{2}$
$T_{sat} [=] K$	$D [=] m$	(All material properties at the film temperature)

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Applied Heat Transfer with Phase Change—Evaporators

Evaporators

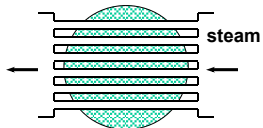
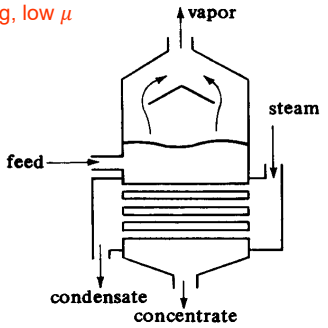
Issues:

- viscosity, m
- scale formation
- liquor velocity
- time in evaporator

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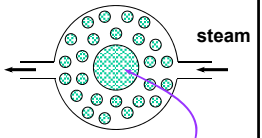
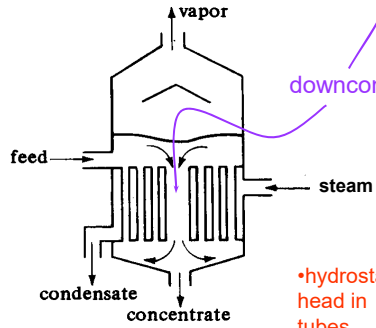
Applied Heat Transfer with Phase Change—Evaporators

- steam in tubes
- liquor on outside
- inexpensive, but poor liquid circulation
- good for non-depositing, low μ fluids

horizontal-tube evaporator

- liquor in tubes
- steam on outside
- liquid circulates by natural convection

vertical-tube evaporator

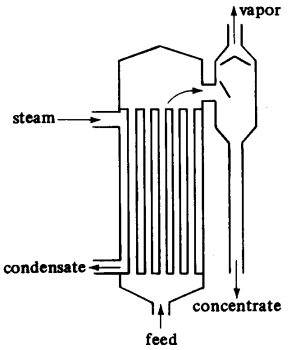
- hydrostatic head in tubes prevents boiling in tubes

Geankoplis, p492
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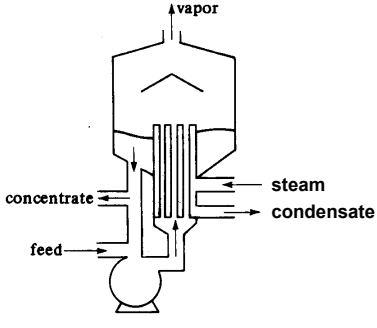
Applied Heat Transfer with Phase Change—Evaporators

- liquor in tubes
- steam on outside
- liquid circulates by natural convection
- single pass
- high liquid velocities



long-tube vertical evaporator

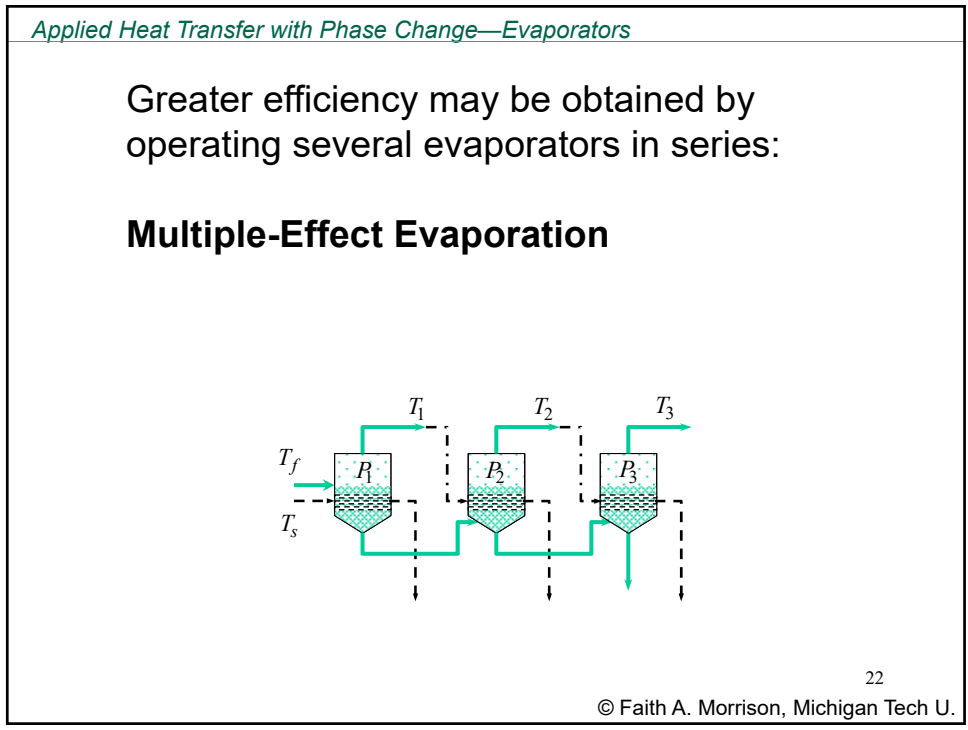
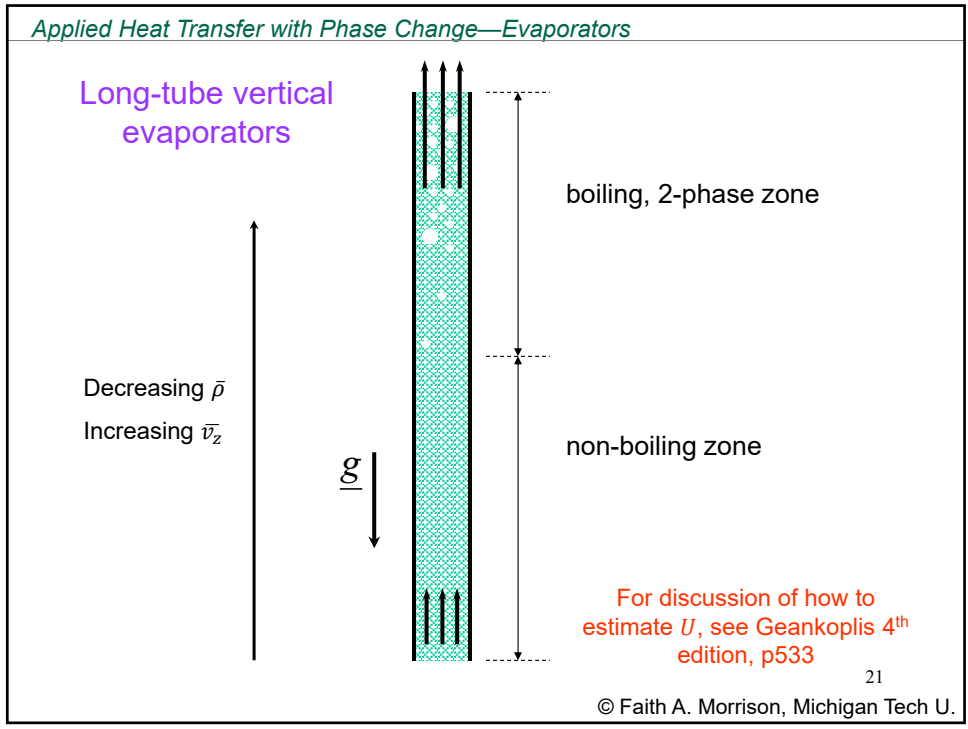
- liquor in tubes
- steam on outside
- liquid circulates by forced convection
- good for high μ fluids



forced-circulation evaporator

Geankoplis, p492
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Applied Heat Transfer with Phase Change—Evaporators

Norbert Rillieux: Inventor of Multiple-Effect Evaporation



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Norbert Rillieux

From Wikipedia, the free encyclopedia

Norbert Rillieux (March 17, 1806 – October 8, 1894), a Creole American inventor and engineer, is most noted for his invention of the **multiple-effect evaporator**, an energy-efficient means of evaporating water. This invention was an important development in the growth of the sugar industry. Rillieux was a cousin of the painter Edgar Degas.

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- 3 Sugar refining
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- 5 Later life
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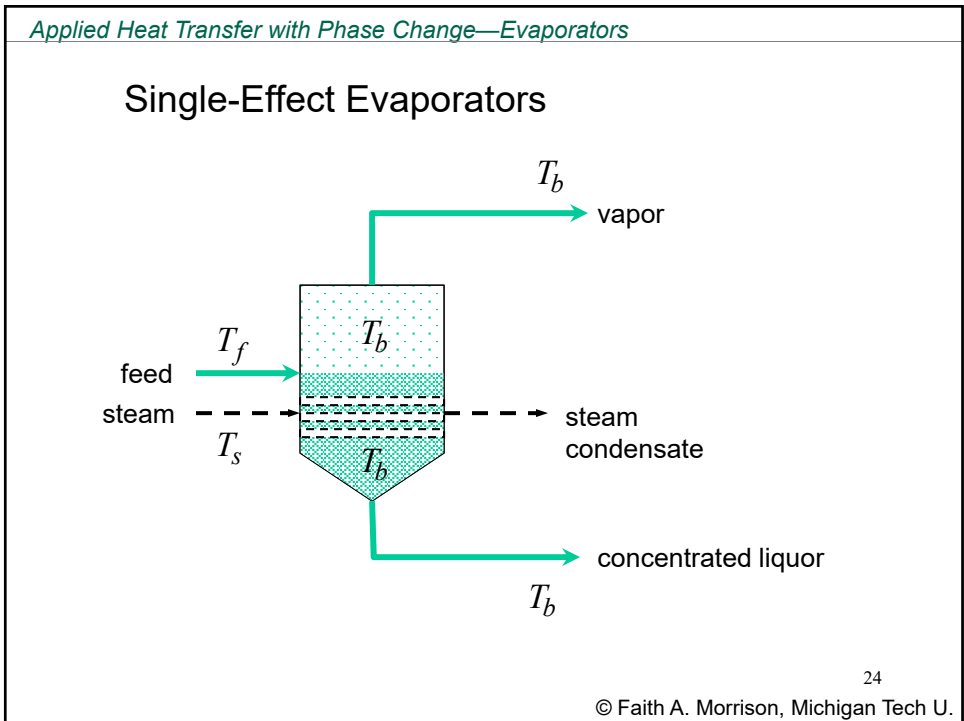
Family [edit]

Norbert Rillieux was born into a prominent Creole family in New Orleans, Louisiana. He was the son of Vincent Rillieux, a white plantation owner, engineer and inventor, and his placée, Constance Vivant, a free person of ...



Norbert Rillieux in an undated photograph

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Applied Heat Transfer with Phase Change—Evaporators

Multiple-Effect Evaporators

For each effect the vapor product becomes the source of heat for the subsequent effect

$$P_1 > P_2 > P_3$$

$$T_1 > T_2 > T_3$$

pressure, temperature decrease

(made white sugar possible)

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Applied Heat Transfer with Phase Change—Evaporators

Compare Single- and Multiple-Effect Evaporators

$$Q = UA(T_s - T_3)$$

$$q_1 = UA(T_s - T_1)$$

$$q_2 = UA(T_1 - T_2)$$

$$q_3 = UA(T_2 - T_3)$$

$$Q = \sum q_i = UA(T_s - T_3)$$

same capacity = same amount of heat transferred
(but we did not have to pay for it all = more efficient)

(used in sugar production, for example)

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Summary

Boiling/Evaporation

- Industrially we operate either in **nucleate** boiling or **film** boiling regimes
- There are different correlations for each regime and for different geometries
 - ✓ Nucleate boiling, horizontal surfaces
 - ✓ Nucleate boiling, vertical surfaces
 - ✓ Nucleate boiling, forced convection
 - ✓ Film boiling, horizontal tube

Condensation

- Industrially we operate in **film** condensation
- There are different correlations for different geometries
 - ✓ Vertical surfaces, laminar or turbulent
 - ✓ Outside stack of horizontal cylinders

Evaporators – designed with the boiling regimes in mind

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Next:

- ~~Heat transfer with phase change~~
- ~~Evaporators~~
- Radiation
- **DONE**

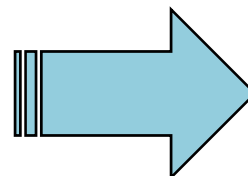
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Radiation Heat Transfer



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