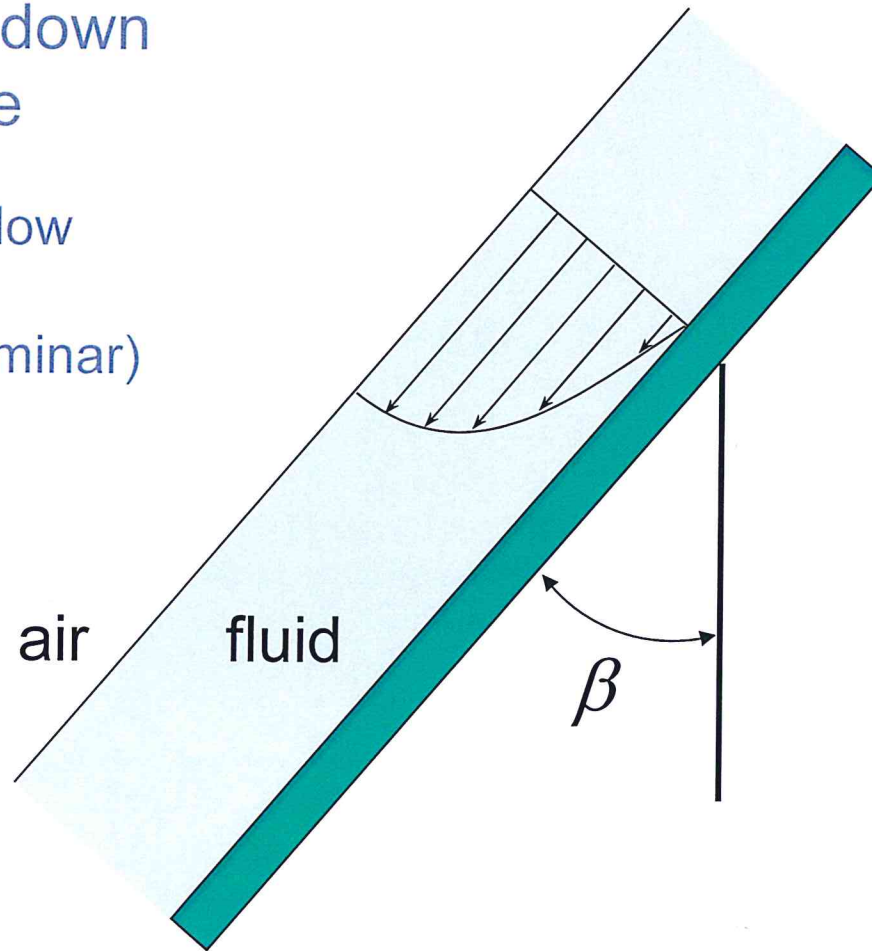


EXAMPLE 1: Flow of a Newtonian fluid down an inclined plane

- fully developed flow
- steady state
- flow in layers (laminar)

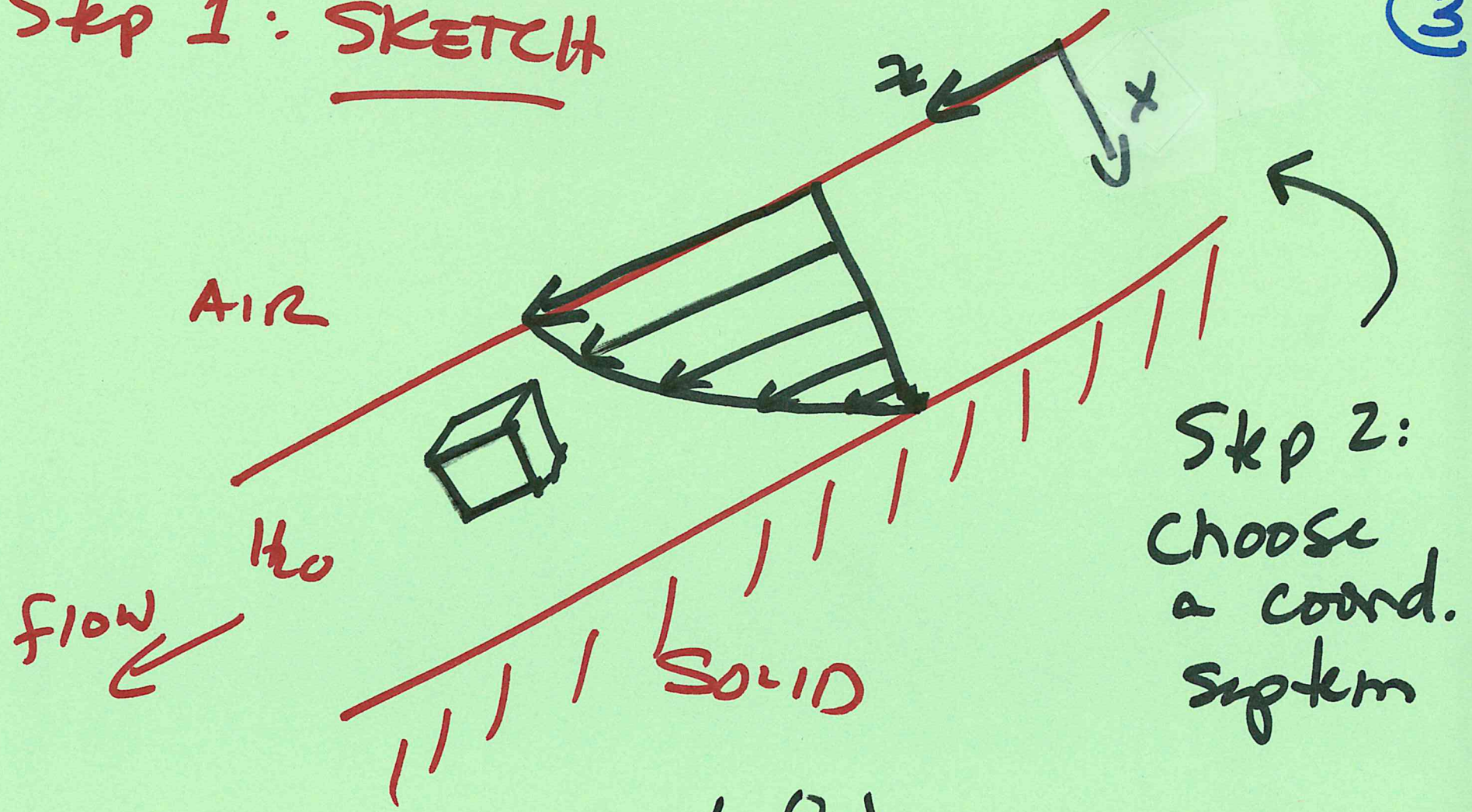


EXAMPLE 1: Flow of a Newtonian fluid down an inclined plane

What is the velocity field in the steady flow of water down a slope that is wide and long. The fluid properties are constant, and the flow is driven by gravity. The flow is slow so that no waves are formed. What is the force on the surface due to the water flow? What is the flow rate?

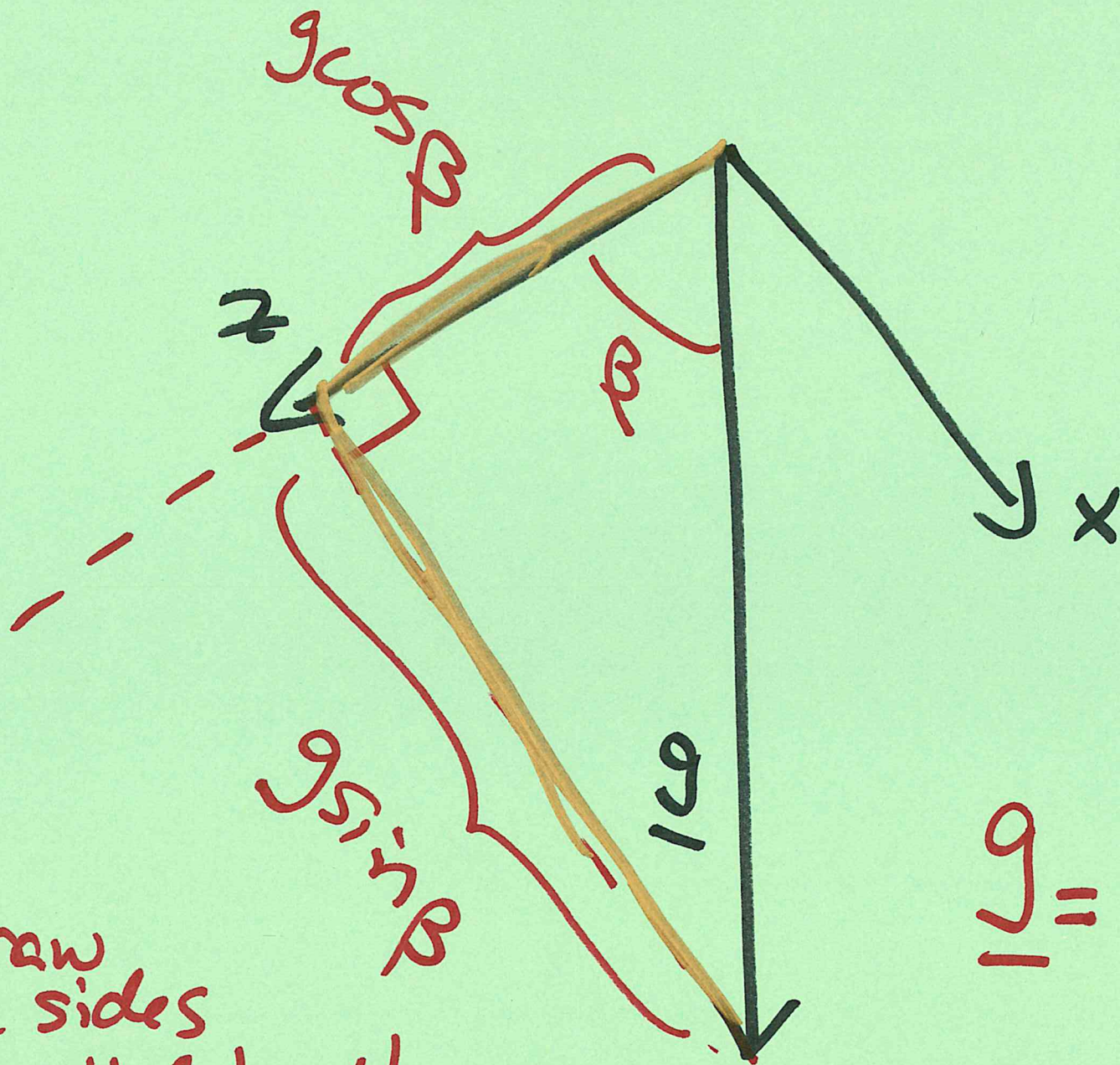
Step 1: SKETCH

3



$$\vec{v} = \begin{pmatrix} 0 \\ 0 \\ v_z \end{pmatrix}_{xyz} = v_z \hat{e}_z$$

DECOMPOSE \underline{g} into our coordinate system. (4)



Draw the sides parallel to the coordinate axes.

$$|\underline{g}| = \begin{pmatrix} g \sin \beta \\ 0 \\ g \cos \beta \end{pmatrix}_{xyz}$$

What are we trying to calculate: ⑤

VELOCITY FIELD

$$\frac{m}{s} (=) \quad \underline{v} = \begin{pmatrix} v_x \\ v_y \\ v_z \end{pmatrix} = \begin{pmatrix} v_x(x, y, z) \\ v_y(x, y, z) \\ v_z(x, y, z) \end{pmatrix}$$

The diagram shows a large red bracket enclosing the vector equation. Inside the bracket, the vector \underline{v} is written as a column vector of v_x , v_y , and v_z . To the right of the equals sign, it is written as a column vector of functions $v_x(x, y, z)$, $v_y(x, y, z)$, and $v_z(x, y, z)$. The variables x, y, z are written below the respective components. There are small arrows pointing to the v_x and v_y components in the first vector, and a larger arrow pointing to the v_z component in the second vector.

- vector
- a function of position

Choose a c.v. that allows you to calc $\underline{v}(x, y, z)$.

MASS

CONTROL VOLUME BALANCES

⑥

→

$$\left(\text{net mass in} \right) = \left(\text{rate of accumulation of mass} \right)$$

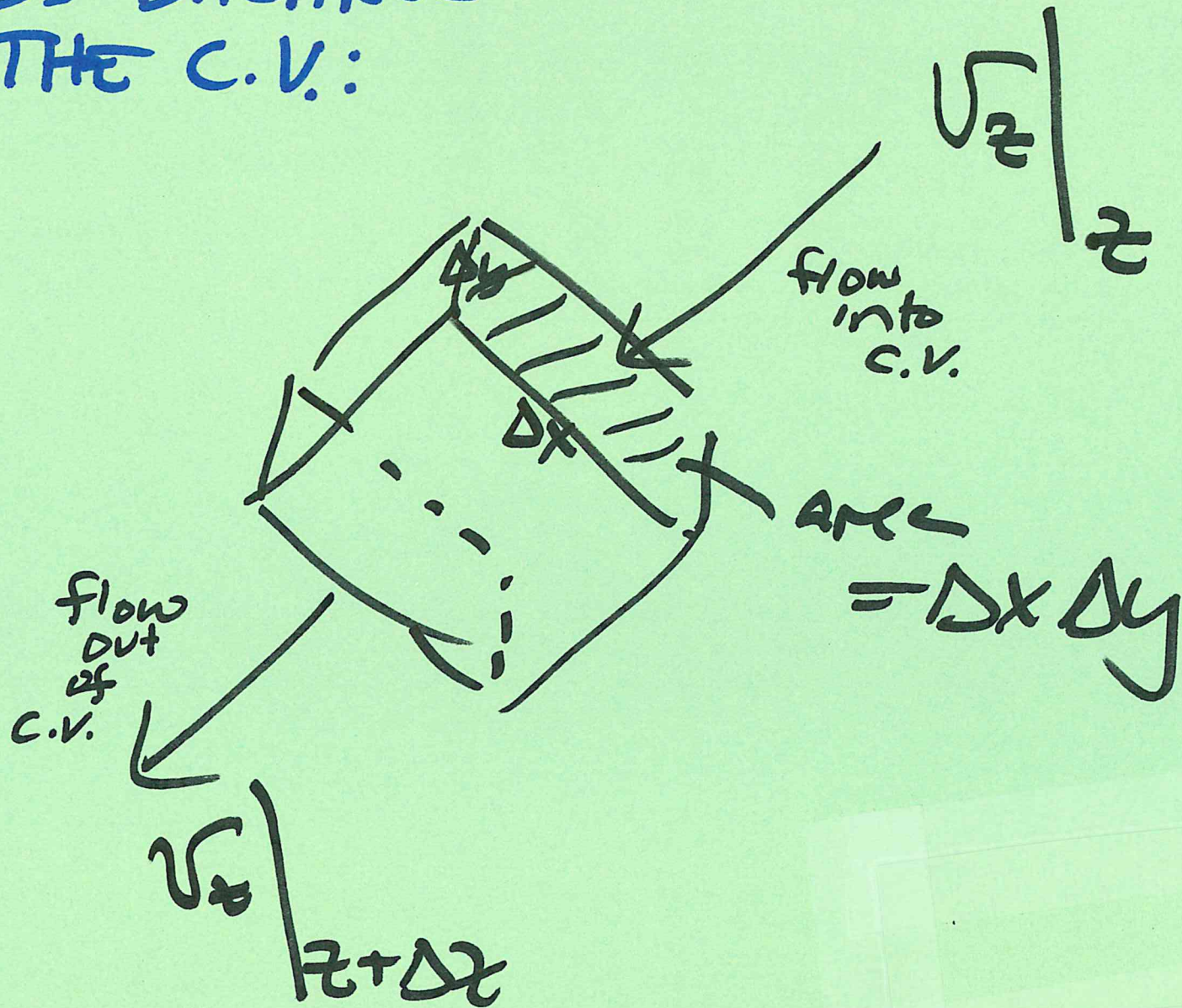
MOMENTUM

↓

$$\left(\text{sum of forces on C.V.} \right) = \left(\text{momentum in C.V.} \right) - \left(\text{momentum out C.V.} \right) = \left(\text{rate of accumulation of momentum in C.V.} \right)$$

"convective terms"

MASS BALANCE ON THE C.V.:



MASS INTO C.V.

Recall: $\langle v \rangle = \frac{Q}{\text{AREA}}$

⑧

$$= \rho \left(\frac{\cancel{\text{Volume}}}{\text{time}} \right) = \frac{\text{mass}}{\text{time}}$$

MASS
in
C.V.

$$= \rho v_z|_z (\Delta x \Delta y)$$

MASS
out

$$= \rho v_z|_{z+\Delta z} (\Delta x \Delta y)$$

MASS IN = MASS OUT

9

$$\cancel{\rho} \cancel{v_z|_z} \cancel{\Delta x \Delta y} = \cancel{\rho} \cancel{v_z|_{z+\Delta z}} \cancel{\Delta x \Delta y}$$

$$v_z|_z = v_z|_{z+\Delta z}$$

$$\lim_{\Delta z \rightarrow 0} \frac{v_z|_{z+\Delta z} - v_z|_z}{\Delta z} = \boxed{\frac{dv_z}{dz} = 0}$$

MOMENTUM BALANCE

(10)

CONVECTIVE TERMS

momentum

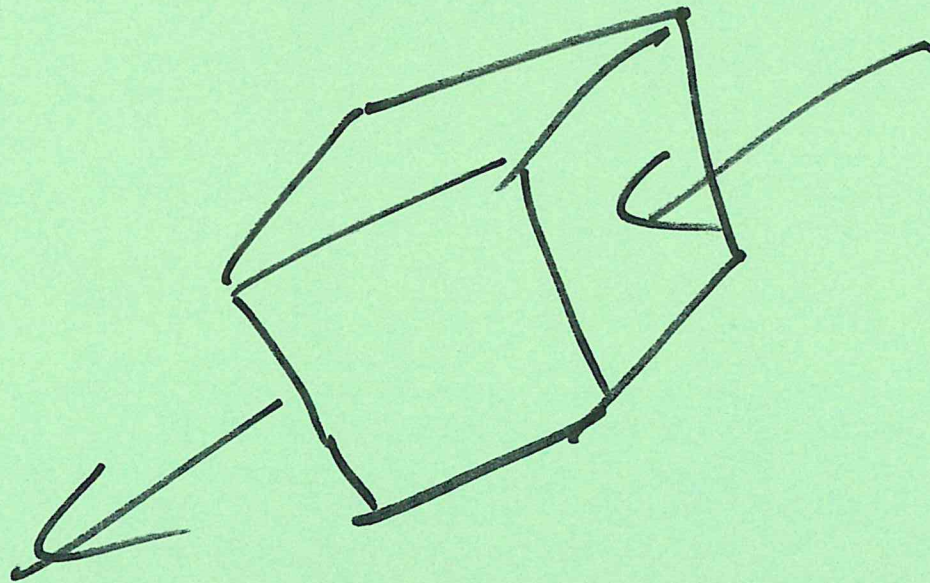
momentum
out ~~into~~
C.V. = $\frac{\text{MASS}}{\text{time}} (\text{velocity})$

$$= \left(\rho v_z \Big|_z \Delta x \Delta y \right) \left(v_z \Big|_z \right)$$

$$= \rho \left(\frac{v_z}{z} \right)^2 \Delta x \Delta y$$

$z+\Delta z$

FORCES - GRAVITY



$$\begin{aligned} \text{Force of gravity on the C.V.} &= (\text{mass})(\text{acceleration}) \\ &= \rho (\text{volume}) g \\ &= \rho (\Delta x \Delta y \Delta z) g \end{aligned}$$

From before:

(12)

$$\underline{g} = \begin{pmatrix} g \sin \beta \\ 0 \\ g \cos \beta \end{pmatrix}_{xyz}$$

(in our
coord
system)

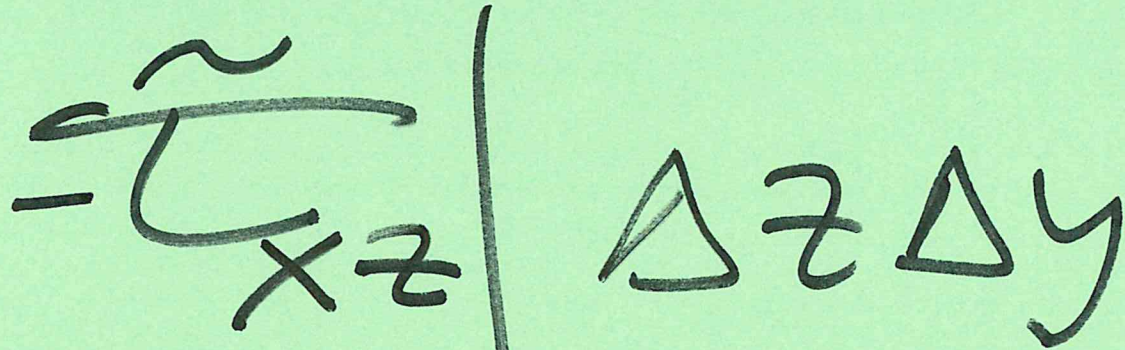
The z -momentum
due to
gravity

$$= \rho g \cos \beta \Delta x \Delta y \Delta z$$

FORCES - VISCOUS

(B)

Force
on
top

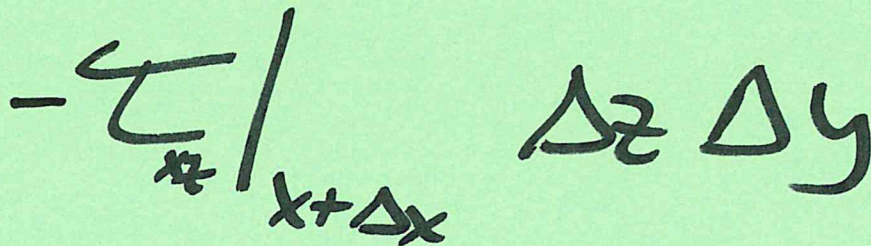


stress on an x
surface in
 z -dir

$$\left(\frac{\text{FORCE}}{\text{AREA}} \right) (\text{AREA})$$

(negative
sign is
to match
stress
sign
convention
of
our
text)

Force on
bottom



$$\rho g \cos \beta \Delta x = \left(-\tilde{\tau} \right)_{x+\Delta x} - \left(-\tilde{\tau} \right)_x$$

Recall: $\lim_{\Delta x \rightarrow 0} \frac{f(x+\Delta x) - f(x)}{\Delta x} \equiv \frac{df}{dx}$

$$\lim_{\Delta x \rightarrow 0} \frac{\left(-\tilde{\tau} \right)_{x+\Delta x} - \left(-\tilde{\tau} \right)_x}{\Delta x} = \rho g \cos \beta$$

$$\frac{d(-\tilde{\tau})}{dx} = -\rho g \cos \beta$$

$$\text{Let } \phi = \tilde{\tau}_{x_2}$$

$$\text{Let } a = -\rho g \cos \beta$$

$$\frac{d\phi}{dx} = a$$

$$\phi = ax + C_1$$

$$\rightarrow \tilde{\tau}_{x_2} = (-\rho g \cos \beta)x + C_1$$

We use Newton's Law of Viscosity to relate $\tilde{\tau}_{x_2}$ to the velocity field.

(16)

(17)

Newton's
Law

of
Viscosity \Rightarrow

$$\tau_{xz} = \mu \frac{dV_z}{dx}$$

Equate:

$$\mu \frac{dV_z}{dx} = -(\rho g \cos \beta) x + C_1$$

$$\frac{dV_z}{dx} = -\frac{\rho g \cos \beta}{\mu} x + \frac{C_1}{\mu}$$

Integrate.

$$V_z = \left[-\frac{\rho g \cos \beta}{\mu} \frac{x^2}{2} + \frac{C_1}{\mu} x + C_2 \right]$$

WE NEED TWO BOUNDARY CONDITIONS

(18)

BC1:

no slip at wall

("at the" wall)

speed = speed of wall

BC1

$x = H$

$(v_z = 0)$

$- \rho g \cos \beta$

$$0 = \frac{\alpha}{2\mu} H^2 + \frac{C_1}{\mu} H + C_2$$

* one eqn, two unknown

SECOND BC.:

BC2: ????

$x = 0$
location

???
condition?

At the "free" surface
(in contact
w/
AIR)

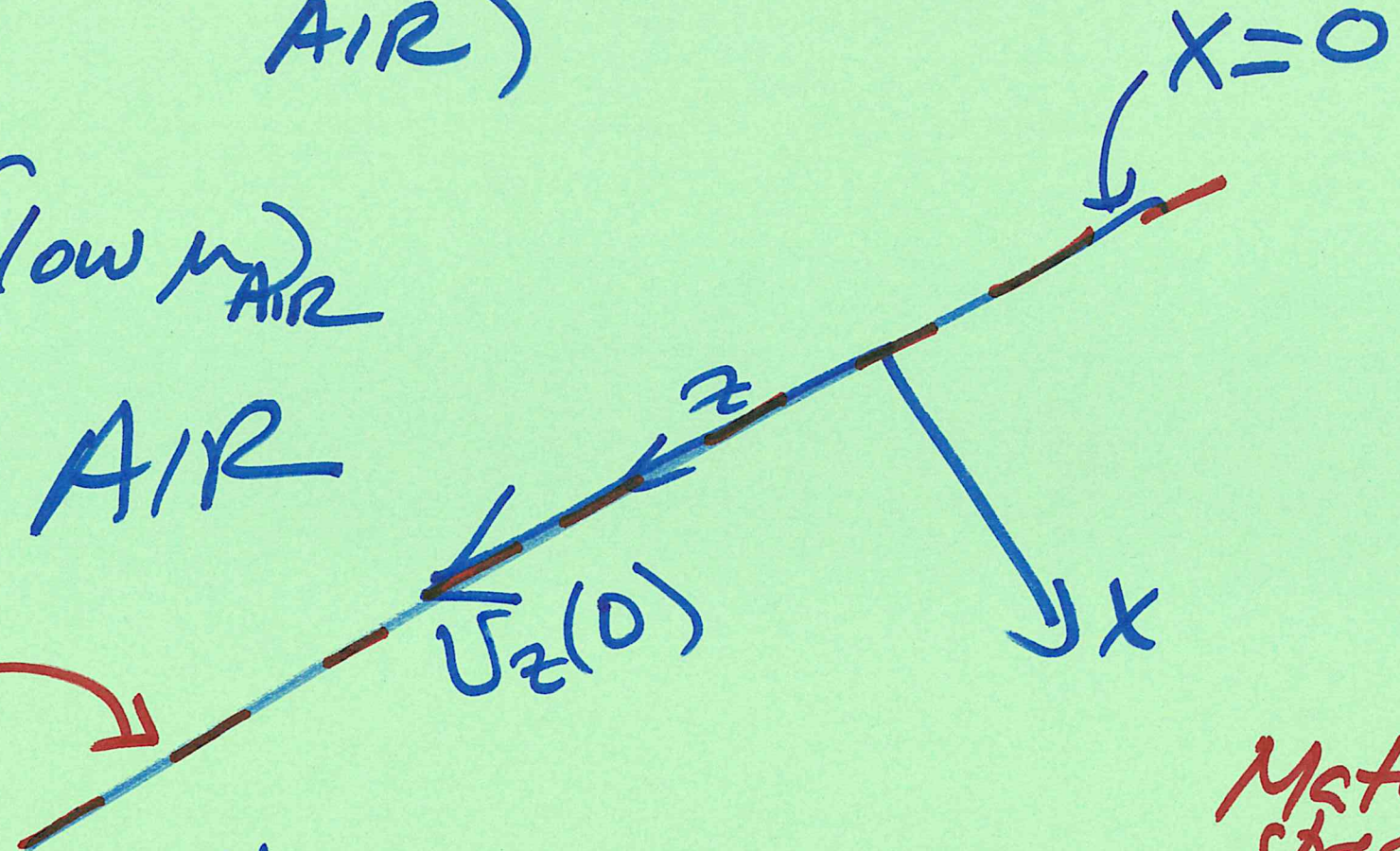
(low μ_{AIR})

AIR

inter-
face

H₂O

μ_{WATER}



Match
stresses
at
boundary

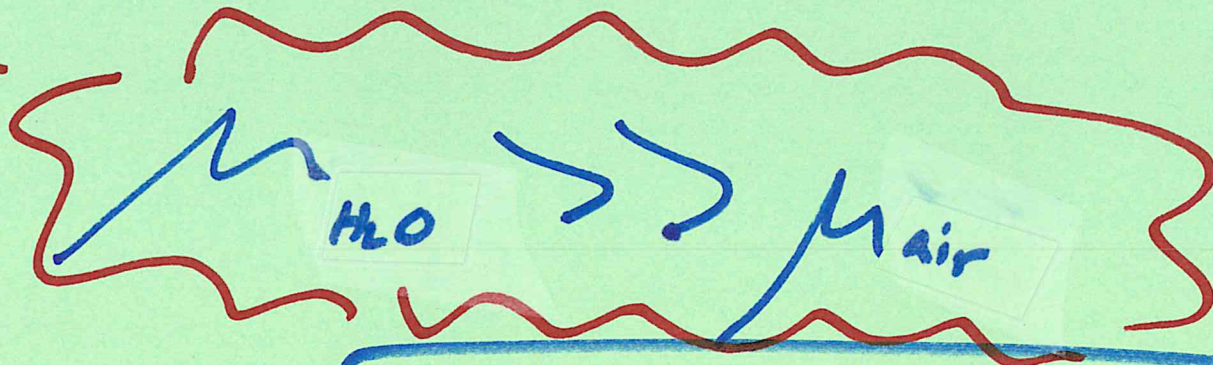
BC 2:

$$x=0 \quad \tau_{xz}^{AIR} = \tau_{xz}^{H_2O}$$

(20)

Newton's Law:

$$0 \approx \mu_{AIR} \left. \frac{dv_z}{dx} \right|_{x=0}^{IN\ AIR} = \mu_{H_2O} \left. \frac{dv_z}{dx} \right|_{x=0}^{IN\ H_2O}$$



\Rightarrow

$$\left. \frac{dv_z}{dx} \right|_{x=0} \approx 0$$

With these two boundary conditions (2)
we are now able to solve 2 eqns,
2 unknowns for C_1 & C_2 to obtain
the final answer for $V_z(x)$.

BC1:
$$0 = \frac{-\rho g \cos \beta H^2}{2\mu} + \frac{C_1 H}{\mu} + C_2$$

BC2:
$$0 = \left. \frac{dV_z}{dx} \right|_{x=0} = \frac{-\rho g \cos \beta}{\mu} (0) + \frac{C_1}{\mu}$$

$$\Rightarrow \boxed{C_1 = 0}$$

$$\Rightarrow \boxed{C_2 = \frac{\rho g \cos \beta H^2}{2\mu}}$$